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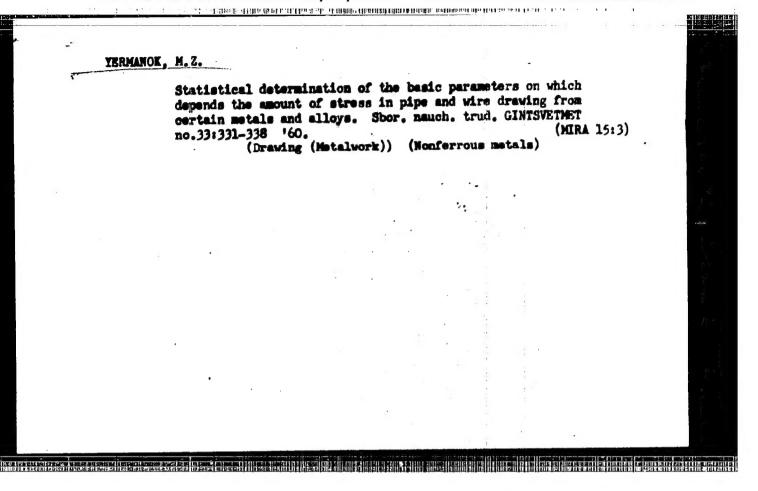
\$/136/60/000/012/009/010 \$193/\$183

Investigation of Stresses During Extrusion of Ribbed Aluminium Alloy Components

between the calculated and factual magnitude of P was only 21%. The general conclusion reached was that if the magnitude of $S_{d.c}$ and K_{kp} for a given alloy is determined experimentally, the extrusion pressure can be calculated with sufficient accuracy with the aid of formula (la). There are 5 figures, 4 tables and 8 Soviet references.

Card 7/7

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31741 \$/136/61/000/012/005/006 \$193/\$383

AUTHORS:

Dontsov, S.N., Yermanok, M.Z., Candidates of Technical Sciences and Chizhov, I.N., Engineer

TITLE:

Strength characteristics of titanium alloys and their application in calculating stresses during plastic-

ह के १४ - १४ तर प्रवास अन-१८ मा अस्ति । रहामधाम वीकामा<mark>सी भरतार ५ मिलक्ष</mark>णकालामणका में मोन्यीय कुरता के में १८ एक ए

work:ing operations

PERIODICAL: Tswetnyye metally, no. 12, 1961, 74 - 76

TEXT: Lack of experimental data on the resistance of Ti alloys to deformation at various temperatures and deformation rates causes difficulties in designing equipment for plastic—working of these materials and in establishing optimum working schedules. Hence the present investigation, which is concerned with the properties of pure Ti (BT| (VT1)) and Ti alloys (BT6 (VT6), BT5 (VT5) and OT4). In Fig. 1, the hot tensile strength (σ_B , kg/mm²) of these materials is plotted against temperature (°C). It will be seen that at 1 050 - 1 150 °C, i.e. in the hot-working temperature range, σ_B of all four materials is very much the same. These values, however, cannot Card $1/\frac{\pi}{2}$

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Strength characteristics of

be used as the basis for calculating stresses during hotworking operations because they represent strength of undeformed material, whereas the strength of an alloy near the exit end of the deformation region depends on the deformation (rolling) rate. The effect of strain rate on $\sigma_{\hat{\mathbf{H}}}$ of the alloys studied is illustrated in Fig. 2, where oh of the alloy VT5 is plotted against test temperature (°C), curves 1-4 relating, respectively, to strain rates of 0.33, 280, 740 and 1 120 %/sec; (similar results were obtained for the alloy VT6). The data presented in Fig. 2 are reproduced in a different manner in Fig. 3, where the so-called strengthming coefficient (c) is plotted against the strain rate (N, %/sec) at temperatures indicated by each curve. If it is assumed that the average resistance of a metal to deformation during rolling. Shop, is an arithmetical mean of its tensile strength near the entry and exit ends of the deformation region, it can be calculated from the formula:

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Strength characteristics of

$$S_{A,CP} = \frac{1+c}{2} \cdot \sigma_{5}$$
 (2)

where first is the tensile strength determined by the Static test at a given temperature and c is the strengthening coefficient corresponding to a given rolling temperature and speed. If, as has been postulated by Perlin, fis a geometrical means of mear the exit and entry ends of the deformation region, Eq. (2) becomes:

$$S_{A,CP} = O_{ETHT} \cdot \sqrt{c}$$
 (3).

The magnitude of c is independent of the rate of deformation in cold-rolling and the average resistance to deformation in this case is simply Card 3/54

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Strength characteristics of

the arithmetical mean of UTS of the alloy before and after rolling. A more accurate value of Spicp in cold-rolling is given by the formula proposed by M.Z. Yermanok in Ref. 5 (IVUZ, Tsvetnaya metallurgiya, 1959, no. 6):

$$s^{\text{D'ob}} = \frac{e^{\text{Had} \cdot \text{Had} \cdot e^{\text{Koh}} \cdot \text{Koh}}}{e^{\text{Had} \cdot \text{Had} \cdot e^{\text{Koh}} \cdot \text{Koh}}}$$
(2)

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where of and of denote, respectively, the UTS of the budy before and after rolling,

FHQH and F denoting the cross-sectional area of the stock at the entry and exit ends of the deformation region.

Card 4/84

"APPROVED FOR RELEASE: 03/14/2001 CIA-RDP86-00513R001962810011-2 5/136/62/000/002/002/004 33165 E073/E135 Zlotin, L.B., and Yermanok, M.Z. 4016 Diagrams for calculating the dependence of the 10.7200 resistance to deformation on the duration and degree AUTHORS: PERIODICAL: Tsvetnyye metally, no.2, 1962, 66-69 A basic parameter for calculating the forces required TITLE: TEAT:

In metal forming is the resistance to deformation 5d; which is greatly influenced by the degree and duration of the deformation. Experimental investigation of these factors is very difficult; also, no standard high-speed experimental equipment is in existence. Therefore various authors attempted to derive formulae for analytical determination of the resistance to deformation during high-speed deformation. In all these formulae the decisive parameter is the speed of the relative deformation. parameter is the speed of the relative deformation is the relative deformation in fractions of unity, where 6 Card 1/4

33165

Diagrams for calculating the ...

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t is the duration of the deformation in seconds. However, the speed of deformation is not a universal parameter; also, the effects of the degree of deformation and the duration of deformation on Sd are not identical. Published data and results obtained by the authors indicate that the influence of the degree of deformation is high, and that it is advisable to take into consideration separately the influence of the degree and the duration of the deformation. The present authors derived a mathematical expression for the influence of the degree and duration of the deformation based on extensive experimental results obtained on the most widely used heavy nonferrous metals and alloys under a great variety of conditions. The Sd versus 1 relations are represented in the form of curves which converge into a single point denoted as the initial resistance to which is the ultimate deformation at the given temperature Sd.H

strength ob determined from static tests. This assumption is based on the following considerations: 1) The yield point does not characterise the resistance to deformation if the deformation

Card 2/4

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Diagrams for calculating the ... S/136/62/000/002/002/004 E073/E135

is predominantly plastic; the force required for plastic stretching or compression is more relevant from this point of view. 2) The real stresses during plastic extension are approximately equal to the strength value and, therefore, it is advisable to use this value as an initial characteristic in the calculations. The authors derived an empirical relation by mathematical statistics methods, using the method of least squares, for determining the coefficients of the sought equation, which is:

$$S_{d.K} = S_{d.H} \cdot a \cdot e^{-b \cdot lg \cdot \tau}$$
 (2)

where a and b are coefficients which depend on the nature of the material, the temperature and degree of deformation. This equation can be transformed into:

$$\lg \frac{S_{\mathbf{d},\mathbf{K}}}{S_{\mathbf{d},\mathbf{H}}} = \mathbf{A} - \mathbf{B} \lg \tau \tag{3a}$$

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In the coordinates $\lg \frac{S_{d,K}}{S_{d,k}} - \lg \tau$, Eq.(3a) can be represented

1913 Progress on a cost. Contract expectations represented to the section of the following manifested the section of the secti

in the form of straight lines, and from this equation diagrams were plotted which converge into a point and permit the determination of $S_{d,K}$. The results are in good agreement with

experiment, the maximum divergence being less than 15%. Analysis of the diagrams plotted in the paper indicates that Eq.(2) reflects the non-identity of the influence of the degree and duration of deformation on the value of S_d. The proposed method was verified by comparison with published experimental results and the agreement was found to be satisfactory. The S_d versus a diagrams reduce considerably the amount of work involved in calculating the value S_d which is required for force calculation in metal forming processes.

There are 3 figures, 1 table and 11 Soviet-bloc references.

Card 4/4

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Yermanok, M.Z. and Shcheglov, G.M.

AUTHORS: TITLE: Extrusion by the inverted and combined method on presses with limited travel of the container

presses with 135 no. 5, 1962, 61 - 65

PERIODICAL: Tsvetnyye metals, A for fabricating aluminium or TEXT: When extrusion is used for fabricating the container, magnesium-alloy sections without lubricating the container, magnesium-alloy sections without lubricating the container much lower extrusion pressures are required if inverted extrusion much lower extrusion pressures narrows considerably in most of the existing extrusion presses narrows considerably in most of the existing extrusion presses narrows considerably in most of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty in extrusion be overcome by using a technique which makes it however, can be overcome by using a techniqu

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Extrusion by the inverted

then moved forward by the extrusion ram 1 and pressure disc until it becomes flush with the front end of the container liner, the container itself being moved back against its stop (Fig. 16). The die head is then brought into position and locked, after which the inverted-extrusion operation is carried out (Fig. 16). As a result of the pressure acting on the billet, the container with the billet advances towards the die head, the dis-holder enters the container liner and the metal is extruded through the die. Movement of the container ceases when the entire length of the die-holder has entered the container and this completes the first stage of the operation (Fig. 12). Further extrusion can be done either by the direct or by the inverted method. In the former case, the entire process will have included both direct and inverted extrusion and can, therefore, be referred to as "combined method of extrusion"; the advantages of this method are demonstrated by data reproduced If the reduction of the extrusion pressure attained in Table 1. by using the combined method is not sufficiently large, the operation, after reaching the stage shown in Fig. 11, can be

Card 2/5

Extrusion by the inverted

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continued by the inverted method, the consecutive singes of which are shown in Fig. 10, e and —. The combined extrusion method was tested by using it to fabricate a most difficult type of extruded section, namely, a section comprising three different profiles, which was extruded with the aid of three split dies. The results indicated that the combined method required an extrusion pressure 625 - 750 tons lower than that required for direct extrusion, which means that both longer billets can be used and smaller cross-section profiles can be made by this method. In addition, the lower temperature of the billet makes it possible to increase the extrusion speed from 0.6-0.7 to 1-1.1 m/min, whereby the efficiency of the process is increased. There are 5 figures and 3 tables.

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Card 3/5

YERMANOK, M.Z.; SHIPILOVA, L.P.

Mechanical properties of semifinished AMg-6 alloy products.

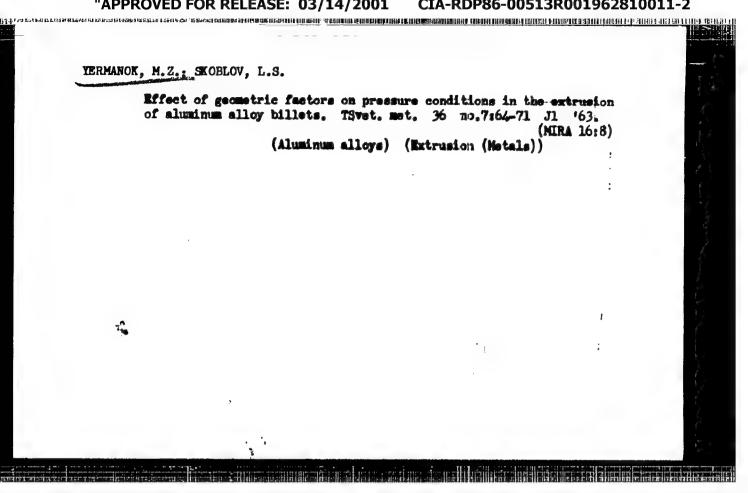
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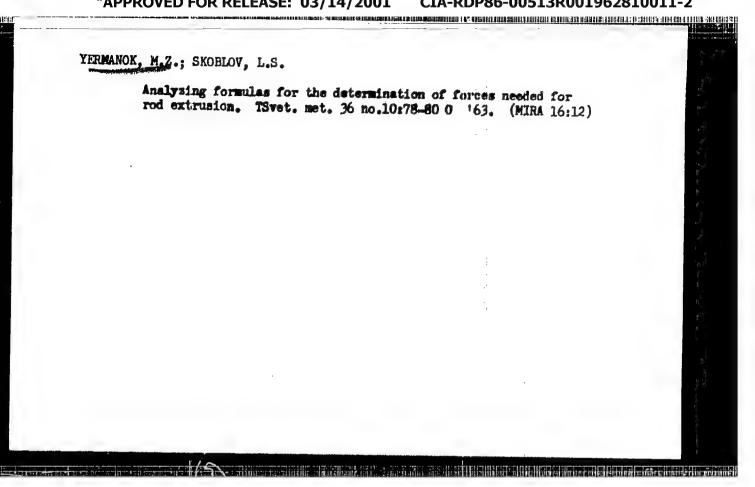
ZACHAROV, M.F.; GLEBOV, Yu.P.; YELMAROK, M.Z.

Pressure conditions in the extrusion of pipe with an arbitrary internal shape. Izv. vys. ucheb. zav.; tsvot. mot. 6 no.3:128-136

(Extrusion (Metals))

(Extrusion (Metals))





ACCESSION NR: AP4030670

8/014:9/64/000/004/0043/0044

AUTHOR: Yermanok, M. Z.; Tomashevskaya, I. M.

TITIE: Influence of preliminary cold deformation on mechanical properties of alloy D16 in tempered pipes

SCURCE: Metallovedeniye i termicheskaya obrabotka metallaw, no. 4, 1964, 43-44

TOPIC TAGS: cold rolled pipe, pipe deformation, pipe strungth, Di6 alloy, cold drawn pipe, tempered pipe

ABSTRACT: Thin walled pipes of D16 alloy made by cold rolling or drawing of a hot forged billet show a degree of deformation from 30-35% to 80-85%, resulting in considerably different mechanical properties. Although this is a very important practical problem, its study has been inadequate. The goal of the authors was to determine the mechanical properties of tempered pipes depending on the degree of deformation prior to tempering. As a result of cold rolling an annealed billet into pipes, their annealing and tempering from 500C in water, the following results were obtained: (1) the wall thickness (1-3 mm) has but little influence on the mechanical properties of D16 alloy pipes; and (2) increasing the rate of cold

Card 1/2

ACCESSION NR: AP4030670

deformation to 70% prior to tempering considerably increases the strength characteristic, and the value of relative elongation corresponds the GOST standard 4773-49. Further increase in deformation does not improve the strength characteristic of pipes. Minimum emounts of preliminary deformation required to reach peak levels of the yield point according to GOST 4773-49 have been established. Originart, has 2 figures, no formulas, no tables.

ASSOCIATION: Name

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Card 2/2

ACCESSION NR: AP4015111

3/0136/64/000/002/0062/0065

AUTHOR: Perlin, I.L.; Glebov, Yu.P.; Yermanok, M.Z.

TITLE: Effect of temperature, degree and rate of deformation on the

deformation strength of aluminum alloys.

SOURCE: Tsvetny metally. No.2, 1964, 62-65

TOPIC TAGS: aluminum alloy, Di6 aluminum alloy, V95 aluminum alloy, AD31 aluminum alloy, deformation strength, deformation rate, deformation temperature, deformation strength temperature function

ABSTRACT: The effect of different temperatures (360, 420, 4800) and various deformation rates (0.19, 0.8, 220 and 880 mm/sec) on the deformation strength S was investigated for D16, V95, and AD31 aluminum alloys. The deformation rate w affects S ; and with increased degree of deformation \(\psi\), the intensity of the growth of S is decreased and in some cases even lowered (for AD31 S is lower at a rate of 14 sec. -/ than at 4 sec. -/). The curves which show the dependence of S on degree of deformation have a maximum, and it is also shown that

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Card 1/8 2

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the degree of deformation depends on temperature and rate of deformation. As temperature increases the maximum on the curve is shifted in the direction of smaller deformation values; and with increasing rate of deformation, it is shifted in the direction of larger deformation values. Working diagrams (fig.1) of the Si = f(t*) relationship were constructed by extrapolation from experimental data for the 3 temperatures investigated. Curves are also included for the most probable deformation periods encountered in extruding the given alloys. The lower curves Siw show the initial values corresponding to Si for has: 3 figures

ASSOCIATION: None

SUB CODE: ML DATE ACQ: 12Mar64 ENCL: 01

SUBMITTED: 00

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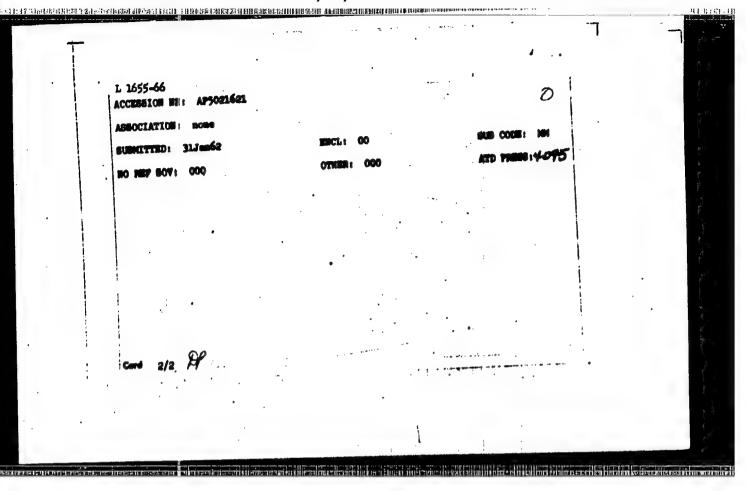
NOSAL', V.V., prof., doktor tekhn.nauk; VERDEREVSKIY, V.A., kand.tekhn.nauk; YERMANOK, M.Z., kard.tekhn.nauk

Review of a book by Z.A.Koffa and others "Cold rolling of pipe." Stal' 24 no.6:536-537 Je '64. (MIRA 17:9)

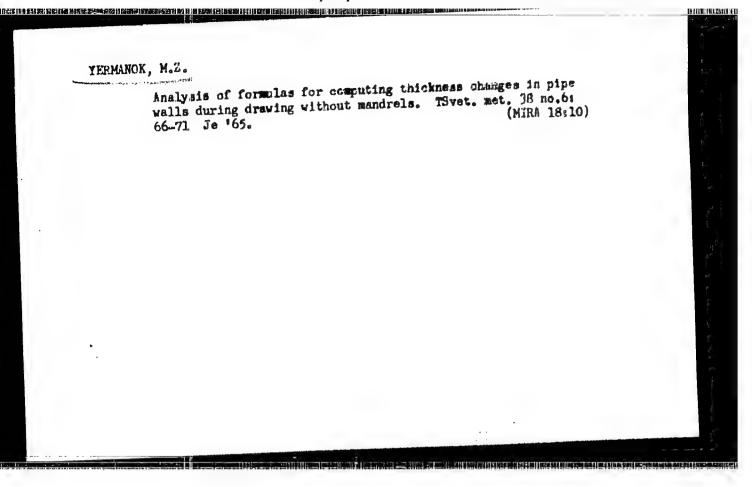
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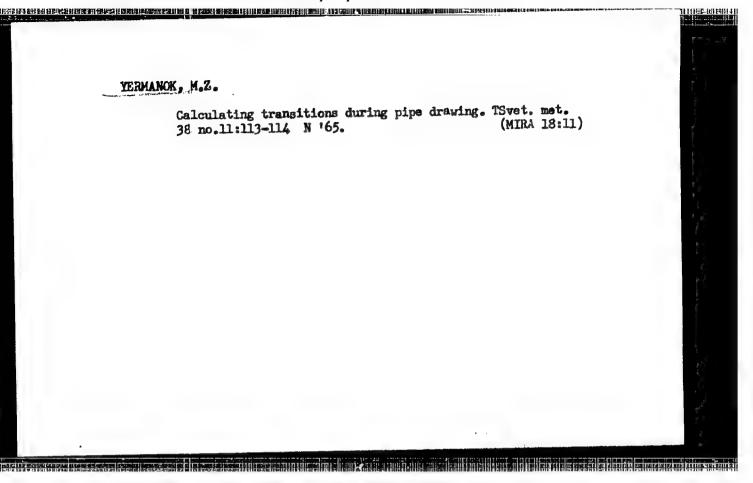
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| | AUTHOR: Shortung, L. A. Coursin, Yu. Y. | y.; Bonbhov. V. M.; Starthov. V. S.; | |
| ł | Rogosinskiy A. A. Langin V. L. Yes | tohin, HAAS; Evitationly, A. S.; 1997) | . 1 |
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| | TITLE: Nother for take extractor Cla | | |
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| | TOPIC TAGS: metal, metal tube, metal o | | |
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| Cord 1/4L | Cord 1/4L | 78.5 | L 1655-66. ENT(d)/ENT(m)/ENP(v)/ENP(t)/ENP(t) JD/MA ACCESSION NR: AP5021621 AUTHOR: Shofmen L. A.; Gedymin, Yu. Yu.; Ro Kryuchkov, M. M. Davrdov, G. Vil Chhaetshin, Bocoinshir, A. A.; Peygin, V. L.; Venorov, I. Rodionov, A. B. 4455 TITLE: Tool for entrading of tubes. Class & SOURCE: Byulleten' isobreteniy i towarnyth; TOPIC TAUE: tube, metal tube, tube entrain ABSTRACT: This Author Certificate introduce solid ingots, i.e., container, mendrel, weld crease the rigidity of individual tools and to one enother, thereby improving the accuration of the container rigidly mounted in relation to the container vided with a central compartment for the importment with the welding chamber, which is mandrel surface. | M. (M.) Starlhov, V. H.; M. W.; Rvichitskiy, A. H.; V.; Roytbarg, L. Kh.; Jerminek, N. J. 9, No. 172602 mekov, no. 13, 1965, 102 p. extrusion tool, extrusion press ing chamber, and die. In order to in- ensure their precise position in relation cory of the extruded tubes, the mandrel is it carries an internal die and is pro- | |
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|------|--|-----|
| - | AUTHORS: Uvarov, V. Ya.; Glebov, Yu. P.; Zhuravlev, F. V.; Surmanol, M. Z.; Rubin, Yu. L.; Zakharov, M. F.; Kochnova, G. P.; Sukhanova, M. P. | 2 1 |
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| - | TITLE: Lubricant for heat treatment of metals. Class 23, No. 173869 (announced by the Organization of Mosgorsovnarkhoz (Organizatsiya mosgo: sovnarkhoza) | |
| | SOURCE: Byulleten" izobreteniy i tovarnykh znakov, no. 16, 1965, 62 | |
| | TOPIC TAGS: lubricant, metal heat treatment, mineral oil | |
| | ABSTRACT: This Author Certificate presents a mineral oil and graphite lubricant for heat treatment of metals. To prevent metals from sticking to the instrument, talcum and red lead are added to the lubricant. The talcum constitutes 10% by weight of the additive, and the red lead constitutes 8-25% by weight. | |
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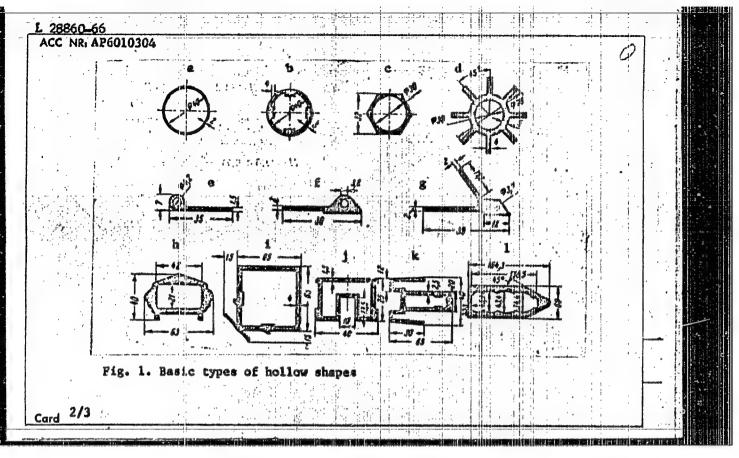
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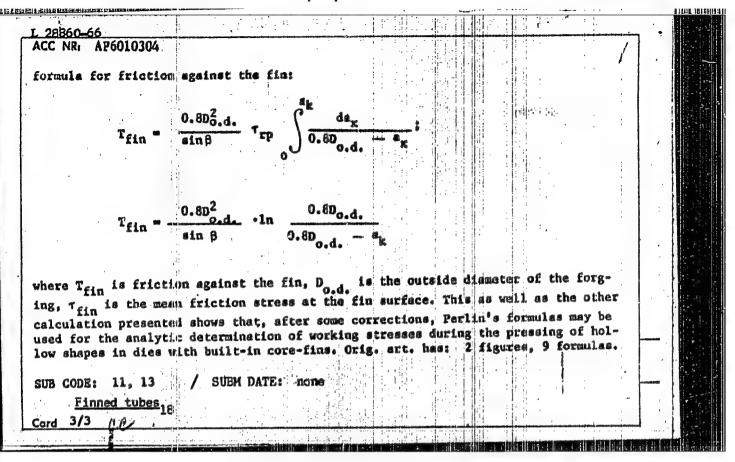
Calculating strain hardening and the temperature field during extrusion. Izv. vys. ucheb. zav.; tavet. met. 8 no.4:134-139 65. (MIRA 18:9)

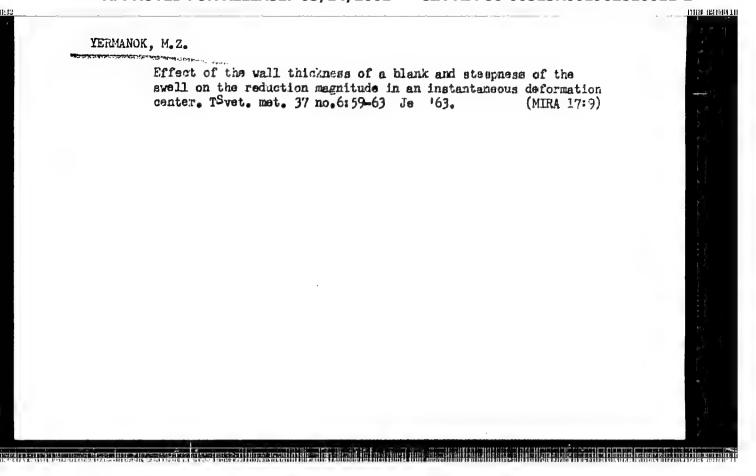
1. Kafedra tekhnologii i avtomatizatsii prokatnogo proizvodstva Moskovskogo instituta stali i splavov.

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| AUTHOR: Yermanok, M. Z.; S | coblov, L. S.; Filing, T | . н. | 49 |
| ORG: none | | | |
| TITLE: Calculation of work with built-in core-fin | ing stresses during pres | saing of hollow shapes | IO GIGB |
| SOURCE: Tavetayye matally, | | | |
| ABSTRACT: The Al and Mg all basic groups (Fig. 1): a, we tubes; b - with cylindrical with shaped external contou (the area of orifice for the with the cross sectional are internal contours. In this sing stress for the pressing pressovaniya metallow. Izdaccount the friction of metallows a triangular prism when | oy shapes forged in core ith cylindrical external external external rand sir and cylindrical intereses 3 groups of shapes es of the shape); h, i, connection, the author of of round tubes in core vo Metallurgiya, 1964), al against the die core sides are friction | a-fin dies may be divided and internal contour haped internal contour hal contour; e, f, g, f, incommendurably small, k, l - with shaped corrects the known for e-fin dies (Perlin, I. since Perlin failed to-fin. Assuming that the | ied into five i, round ; c, d - loop type ll compared external and mulas of pres- L. Taoriys o take into is fin repre- |

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8/125/60/000/012/004/014 A161/A030

AUTHORS: Brodskiy, A.Ya; Fridman, A.M; Yermanck, Ye.Z; Frolov, S.A.

TITLE: Resistance Welding of 30Kh02S Reinforcement Steel for Pre-Stressed Reinforced Concrete Structures

PERIODICAL: Avtomaticheskaya svarka, 1960, No. 12, pp. 28 - 36

TEXT: The weldability of 30X Γ 2C (30KhG2S) reinforcement steel in resistance welding machines has been investigated and practical recommendations are given. The standard composition of this steel (GOST 5058-57) is: 0.26 - 0.35% C; 0.6 - 0.9% Si; 1.2 - 1.6% Mn; 0.6 - 0.9% Cr; not above 0.3% Ni and Cu (each): the mechanical properties: conditional yield limit $\sigma_{0.2} > 60 \text{ kg/mm}^2$; ultimate strength $\sigma_{0.2} > 90 \text{ kg/cm}^2$; elongation $\sigma_{0.2} > 60 \text{ kg/mm}^2$; ultimate around a mandrel with diameter equal to 3 diameters of the tested rod. Rods used for experiments were periodical, with 1^{14} - 28 mm diameter, produced by the Stalino and Magnitogorsk metallurgical works. Round test specimens with sharp notch in different heat affected zones, so-called UHN Π C(TanIPS specimens) were used with success first or all with other reinforcement steel, but had to be replaced with Menazhe (Russian transliteration) notch specimens for 30KhG2S because of its very high notch sensitivity. It proved also very sensitive to inaccuracy of connection Card 1/4

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S/125/60/000/012/004/014 A161/A030

Resistance Welding of 30KhG2S Reinforcement Steel for Pre-Stressed Reinforced Concrete Structures

angle in cross connections as well as to burns in machine grips during resistance welding. It is recommended to prevent burns by using electrodes with a wide contact surface, to raise the gripping effort, to carefully clean the surface of electrodes and rods, and to reduce the current density in these spots, which is possible by not only conducting current to the bottom electrodes but also to the upper hold-downs made from copper alloy. In view of the high sensitivity to heating time with butt welding, preheating should be carried out, (not too drastically) - e.g. continuous fusing is not premissible - for chilling in the heat-affeeted zone reduces strength through the formation of martensite spots (Fig. 3) which affects deformability and thus causes cracks. The formation of martensite can be prevented by heat treatment between the electrodes of resistance welding machines fitted with special automatic devices. [Abstracter's note: No details of such devices are mentioned]. The optimum welding process conditions were found in experiments in an ACM\$\phi\$-75 (ASIF-75) welder with a recorder which enabled the duration and temperature of preheating, the magnitude of upsetting, the number of preheating cycles, and the total welding time to be determined. The optimum values of the following major parameters were determined: setting length 1 yCT Card 2/4

S/125/60/000/012/004/014 A161/A030

Resistance Welding of 30KhG2S Reinforcement Steel for Pre-Stressed Reinforced Concrete Structures

fusion length $l_{OD,\Lambda}$, and upsetting length l_{OC} , as well as the transformer stage. The optimum process was determined by the shape of the curves of breaking load, bending angle and impact strength in butt joints. For medium-diameter reinforcement rods the lycr , long and loc values must be 2.8; 0.7 and 0.35 respec-Joints in 20 and 28 mm diameter rods were tively. Butt d so welded in ASIF-75 and Mcp-100 (MSR-100) welders. In spot welding of cross joints the weldability of 30KhG2S steel was much lower than of Cr.5 (St.5), and the highest possible mechanical strength was obtained with about 2 sec. holding (St.5 requires three times as much holding). With St.5 rods, spot welded connections can be obtained with mechanical strength not below the strength of the base metal, regardless of the transformer stage, but in 30KhG2S spot welds the strength can drop drastically and be very uneven. The cause is the presence of martensite and heterogeneous structure. The properties of cross joints can appearantly be improved by heat treatment in the welding machine (between electrodes) (Ref. 3) (A. Ya. Brodskiy, P.I. Sokolovskiy. A.M. Fridman, "Avtomaticheskaya svarka", No. 3, 1958). Conclusions: 1) Resistance welding with 30KhG2S reinforcement steel is more difficult than with other Soviet reinforcement steel grades, but butt joints Card 3/4

3/125/60/000/012/004/014 A161/A030

Resistance Welding of 30Kh02S Reinforcement Steel for Pre-Stressed Reinfor ed Concrete Structures

are possible with ultimate strength not below the standard minimum for this steel. 2) Smooth (r.3 (St.3) steel rods can be joined with 30KhG2S rods by spot welding into cross joints without weakening the rods. Cross joints of 30KhG2S with 30KhG2S have not more than 86% of initial metal strength before welding. 3) Brittleness is the drawback of all joints in 30KhG2S steel rods made by resistance welding, but it may be eliminated by heat treatment between electrodes. There are 6 figures and 3 Soviet references.

ASSOCIATIONS: Tanil stroitel nykh konstruktsiy ASiA SSSR (Tanil of Construction Frameworks AS and A USSR). A.Ya. Brodskiv and A.M. Fridman; NII zhelezobeton pri Mosgorispolkome (Scientific Research institute for Reinforced Concrete at Moscow City Executive Committee), Ye.Z. Yermanok: MVTU imeni Baumana (MVTU imeni Bauman), S A Frolow

SUBMITTED:

March 3, 1960

Card4/4

| AUTHORS: Yermanok, Y | e. Z.; Rodin, I | Z, : Sluvariko | v. V. M., Granivsk | 55 11. B. T. | |
|---|---|--|---------------------|-----------------|---|
| TITLE: A method for | | | | 336 | |
| SOURCE: Byulleten' i TOPIC TAGS: welding, | • | | | nology, are | |
| welding | | | | 1 | 1 |
| ABSTRACT: This Author between rods and plat the welded joint, the of an electrode provide | s. To facilitat heading is produ | te the process ar | id to imirove the o | uality of | |
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| ABSTRACT: This Author between rods and plat the welded joint, the of an electrode provide | es. To facilitat heading is produ ied with a groove | te the process ar iced in the cours | id to imirove the o | uality of | |

Card 1/1 Pub. 124 - 20/28

Authors : Pogodin A. S., Eng.; Bulatov, N. I. Tormanov, B. V., Ing.; and Eurkov, V. I., Eng.

Title t Problems dealing with a non-mimsograph method of approducing drawings

Periodical : Vest. mesh. 35/6, 75 - 80, Jun 1955

Abstract : A series of latters submitted to the editor of this publication by implication

| Region of the second of the se | No. of the second secon | [1] A. M. Martin, Phys. Rev. B 48, 127 (1997). | 1 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 |
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18(7) S

SOV/32-25-4-24/71

AUTHORS: Yermanovich, N. A., Longinov, M. F., Orlov, L. G., Utevskiy, L.M.

TITLE: Examination of Interdendritic Nonmetallic Streaks in Cast Steel (Obnaruzheniye mezhdendritnykh nemetallicheskikh prosloyek v

littoy stali)

PERIODICAL: Zavodskaya Laboratoriya, 1959, Vol 25, Nr 4, pp 440-442 (USSR)

ABSTRACT: Sites of fracture in some structural steels (40 KhNMA, 12Kh2N4A,

30KhVFYu, 30 KhGSA, 30 KhGSNA) pointed to a destruction of the metal along the boundary of the primary grain. On the strength of tests it is assumed that nitrides, especially aluminum

nitride (I), accumulate at these boundaries and produce a weakening. This assumption was examined in the present case by means of an electron microscope and an electronograph. By an electrolytic heating, a thin coating layer was obtained at the site of fracture, which could be removed by the reagent according to Popova and examined. On the microphotograph of a

fracture in the steel 40 KhNMA (Fig 1) one can well observe the inclusions, the forms of which are represented even better by

the electron microscope (Fig 2). The phase composition of these inclusions was investigated by the X-ray structure- and electro-

Card 1/2 nographic method. In the X-ray picture (I) was observed in the

SOV/32-25-4-24/71

Examination of Interdendritic Honmetallic Streaks in Cast Steel

steel 38 KhVFYu (I), and (I) and VN in samples with big faults, (I) and F₃Al₂(SiO₄)₃ in the steel 12 Kh2N4A - (I), and (I) in the steel 40 KhNMA - (I). The electronograms (Fig 3 for 40KhNMA) corresponded to a crystal lattice of (I). In order to convert structural components from a disperse to a crystalline form, the samples were treated in the vacuum (at 800° for 2 hours); a fine formation of stains (Fig 4) was observed and the distinct electronogram of a polycrystal (Fig 5) was obtained with three phases - a spinel lattice, (I) and a phase which could not be identified. A test storing in the vacuum at room temperature for some days showed a crystallization, the electronogram of which is described (Table). There are 5 figures and 1 table.

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ASSOCIATION:

Zlatoustovskiy metallurgicheskiy zavod, Tsentral'nyy nauchnoissledovatel'skiy institut chernoy metallurgii (Zlatoust Metallurgical Works, Central Scientific Research Institute of Iron Metallurgy)

Card 2/2

18 (7) AUTHORS:

Longinov, M. F., Yermanovich, N. A.

SOV/32-25-5-17/56

TITLE:

Separation and Analysis of Steel Impurities (Razdeleniye i

analis vklyucheniy v stali)

PERIODICAL:

Zavodskaya Laboratoriya, 1959, Vol 25, Nr 5, pp 571-573 (USSR)

ABSTRACT:

A method is described, which allows a separation of the steel impurities (I) from the carbides (II) without a chemical treatment of the anode precipitate as well as a separation of (I) in individual phases for the X-ray structural and electronographic analysis. For this purpose the authors comminuted the anode precipitate soaked in alcohol with an electromagnetic vibrator (Fig 1) for 2-3 hours. The (II) whose dispersity is considerably higher remain dispersed and thus oun be separated from the deposited (I). The ferromagnetic phase is then separated from (I) with a magnet and the other phases are separated according to the specific weight. The latter may take place mechanically with a special apparatus (Fig 2) on which the interaction between centrifugal force and gravity is made use of. To be true, this method does not allow the separation of (I) having a dispersion degree equal to that of (II). This, however, can be attained by a continuous

Card 1/2

APPROVED FOR RELEASE: 03/14/2001 CIA-RDP86-00513R001962810011-2"

Separation and Analysis of Steel Impurities

SOY/32-25-5-17/56

decarbonization of steel up to a low carbon content, in which case the total carbon passes over into the solid solution during hardening of the sample and no (II) is formed. This decarbonization of the sample takes place in a closed tube (Fig 3) which is kept at 1150-1250° during 80-100 hours. In this way sulphides (CuS, MnS), oxides (MgO, Al₂O₃) nitrides (AlN, VN) could be determined in the steel 40 KhNMA. It was proven that at the grain boundaries in the steel 30 KhVFYu mitrides (AlN, VN) having a pink and blue coloring may be found. In steel 12 KhMF large amounts of copper sulphide steel impurities (Fig 4) were found and the angular c ystals observed in steel Kh 17 N 2 were identified as MgAl₂O₃ crystals. There are 4 figures.

ASSOCIATION:

Zlatoustovskiy metallurgicheskiy savod (Zlatoust Metallurgical Plant)

Card 2/2

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S/130/63/000/003/001/001 A006/A101

AUTHORS:

Khasin, C. A., Yermanovich, N. A., Pribytkova, K. N.

TITLE:

Improving the ductile properties of high-chromium steels

PERIODICAL: Metallurg, no. 3, 1963, 27 - 29

TEXT: The authors studied the effect of hot deformation temperature, cooling methods after rolling, and variants of heat treatment upon the ductile properties of high-chromium steels. Square and round specimens were subjected to the following variants of forging, heat treatment and cooling: preheating for forging from 1,000 - 1,200°C; forging completed at 700 - 940°C; heat treatment at 780 and 900°C during 4 hours; quenching in water and air. It was found that the ductility of steel, determined from the magnitude of contraction after forging, increased with lower forging temperatures. A considerable increase in ductility occurs when the temperature of completed forging is below 800°C. There was no marked difference between the properties of metals, cooled after forging in air, water and cinder. Heat treatment of forged metal at 780°C for 4 hours and cooling in water raises considerably the ductility of the steel and is re-

Card 1/2

S/130/63/000/003/001/001 Improving tin ductile properties of high-chromium steels A006/A101

commended for steels which do not possess the required ductile properties after forging and rolling. Changes in the microstructure, depending upon heat treatment conditions, were studied by heating square steel specimens to temperatures

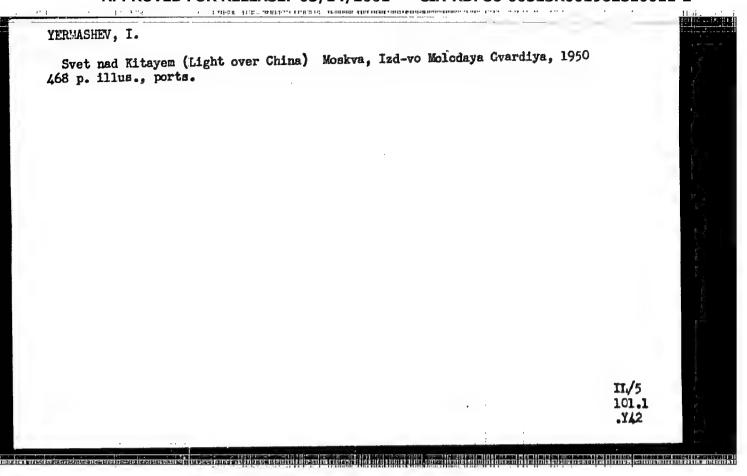
ranging from 700 - 1,100°C with different holding time, and dooling with the furnace, in air or in water. After heat treatment at over 800°C, the ductile properties of the steel remain low; they are normal at 780°C heating for 4 - 5 hours. There are 3 figures and 2 tables.

ASSOCIATION: Zlatoustovskiy metallurgicheskiy zavod (Zlatoust Metallurgical Plant)

Card 2/2

PERLIN, I.L.; OLEBOV, Yu.P.; YERMANYUK, M.Z.

Character of the dependence of the resistance to deformation on the degree of deformation in recrystallization processes following the pressure working of metals. Inv. vys. ucheb. sav.; tsvet. met. 7 no. 4:135-141 764 (MIRA 19:1)



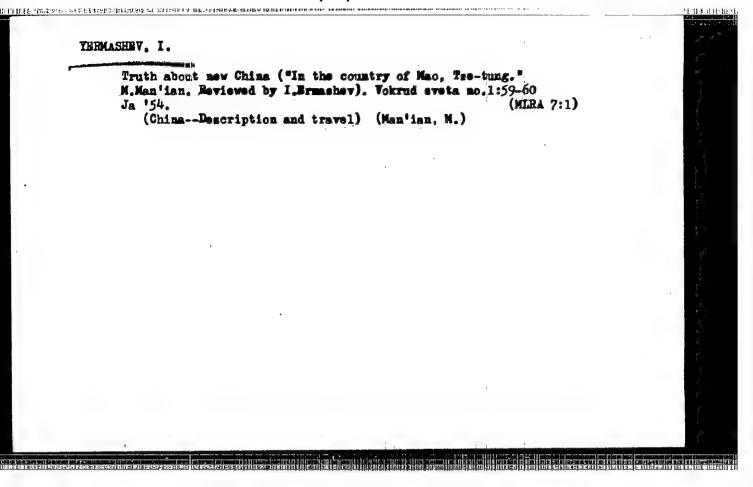
YERRASHEV, I.

Tibet

New book about Tibet ("Tibet". B. V. Yusov. Reviewed by I Yermashav.) Vokrug sveta, no. 8 1952.

2

9. Monthly List of Russian Accessions, Library of Congress, November 1973, Uncl



MARKOV, N.M., kand.tekhn.nauk; TERENT: YEV, I.K., kand.tekhn.nauk; TERMASHOV, N.N., insh.

Some results of the experimental study of the effect of steam moisture on the characteristics of turbine stages. Izv. vys. ucheb. zav.; energ. 6 no.3:68-74 Mr 163. (MLRA 16:5)

1. TSentral nyy kotloturbinnyy institut imeni I.I.Polsunova. Predstavlena sektsiyey parovykh i gazovykh turbin. (Steam turbines)

APPROVED FOR RELEASE: 03/14/2001 CIA-RDP86-00513R001962810011-2"

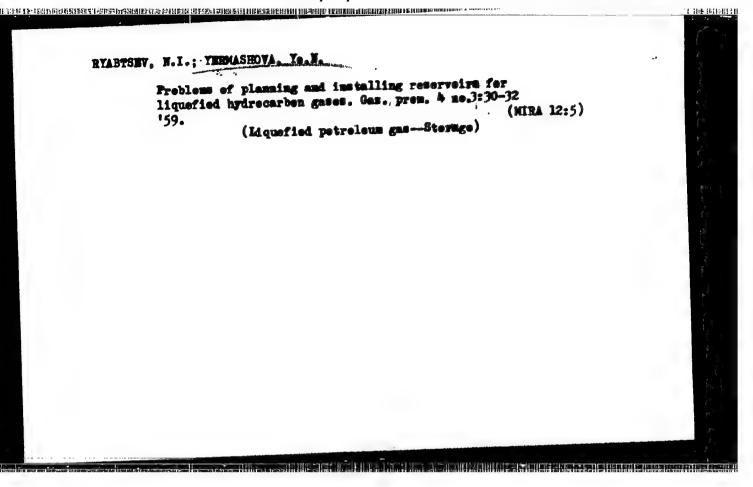
(MIRA 18:9)

YERMASHOV, N.N., inzh.; MARKOV, N.M., doktor tekhn. nauk, prof. Development of instruments for determining the degree of steam moisture. Izv. vys. ucheb. zav.; energ. 8 no.8:96-100 Ag '65.

1. TSentral'nyy kotloturbinnyy institut imeni I.I. Polzunova.

RYADTSEV, N., kand.tekhn.nauk; YERMASHOVA, Ye., insh.

Using liquefied hydrocarbon gases for compensating daily and seasonal fluctuations and substituting other gases. Zhil.-kows. khos. 8 no.1:12-15 '58. (MIRA 11:1) (Gas distribution)



66473

21(8) 5.4500(B)

SOV/20-129-1-19/64

AUTHORS:

Starodubtsev, S. V., Academician, Academy of Sciences, UzbekskayaSSR, Ablyayev, Sh. A., Yermatov, S. Ye.

TTTLE:

Variation of Adsorptive Properties of Silicagel Under the

Action of Gamma-irradiation

PERIODICAL:

Doklady Akademii nauk SSSR, 1959, Vol 129, Nr 1,

pp 72 - 73 (USSR)

ABSTRACT:

Ionisation and excitation of atoms and molecules as well as displacement of the atoms is caused in solids under the action of penetrating rays. It becomes manifest by an external variation of the mechanical, optical, electrical, physico-chemical, and chemical properties of the bodies. Different preliminary works dealing with this subject are shortly reported. The properties of irradiated silicagel have hitherto been investigated only by A. N. Terenin et al (Refs 6,7). These authors irradiated silicagel by ultraviolet

rays and showed, that a process occurs, similar to that on heat treatment, i. e. hydroxyl groups are separated and free valences occur at the surface. Present paper describes the experimental investigation of adsorptive properties,

Card 1/3

APPROVED FOR RELEASE: 03/14/2001

CIA-RDP86-00513R001962810011-2"

Variation of Adsorptive Properties of Silicagel SOV/20-129-1-19/64 Under the Action of Gamma-irradiation

basing on the adsorption of gases, measured by means of thermocouples and ionization manometers. Experimentally produced silicagels of the type KSK were used for this experiment. Prior to the investigation, these silicagels were subject to careful, long lasting heat treatment, and were then irradiated by Y-rays (dose rate 15.104 to 35.104 r/hour, total dosage 1.5.106 to 2.106 r) in evacuated glas tubes (which were provided with manometer tubes). The following is shown by the results of these investigations: The adsorptive power of silicagel increases remarkably under the influence of Y-rays, and the amount of the gas, adsorbed by the irradiated Silicagel increases up to a known boundary value, with increasing irradiation dose. The first diagram shows the change of the adsorptive properties of silicagel with respect to H2, N2 and Ar at low pressures, and the second diagram shows the same for CO2, CO, NH3, C2H4 and H2S, under the condition, that pressures of 1 - 10-1 torr prevailed before the irradiation. According to these diagrams, the adsorptive power of the irradiated silicagel samples increases differently for different gases.

Card 2/3

66473

Variation of Adsorptive Properties of Silicagel Under the Action of Gamma-irradiation

SOV/20-129-1-19/64

At comparatively high gas pressures (4 torr) the irradiated silicagel can adsorb an amount of hydrogen of 2.5.10-5 of its total weight. In this experiment, it is important and interesting, that silicagel assumes its previous properties, if heated to 100°. At room temperature, almost no such "annealing" of the irradiation effect may be noticed. Obviously, the changes of the adsorptive properties of silicagel under irradiation with y-rays may be explained by the separation of hydroxyl groups and the formation of free valences at the surface as well as by the interruption of the bonds between the free radicals (which were formed during the primary heat treatment) and by the high ionization of the gas (the adsorbate), effecting an increase of the adsorptive power of silicagel. There are 3 figures and 7 references, 6 of which are Soviet.

SUBMITTED:

June 9, 1959

4

Card 3/3

33100 \$/638/61/001/000/025/056 B104/B138

5.4600

AUTHORS: Ablyayev, Sh. A., Yermatov, S. Ye., Starodubtsev, S. V.

TITLE: Variation in adsorption properties of silica gel during

gamma irradiation

SOURCE: Tashkentekaya konferentsiya po mirnomy ispol zovaniyu atomnoy

energii. Tashkent, 1959. Trudy, v. 1. Tashkent, 1961,

This is the charge at the figure of the contract of the contraction of

174 - 177

TEXT: The adsorption properties of industrial KCK (KSK) silica gel were determined from the amount of gas absorbed, and by measurements with thermocouple and ionization manometers. Before the experiments, the samples were carefully heat-treated, sealed in evacuated ampoules, and exposed to gamma rays. Radiation dose was 150 - 350,000 r/hr reaching a total of up to 2 million r. The adsorption properties of silica gel increase considerably during irradiation, and differ for different gases. Some gases, such as argon or hydrogen sulfide, are hardly adsorbed at all. Amounts of gas additionally adsorbed during irradiation:

Card 1/3

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33100 \$/638/61/001/000/025/056 B104/B138

Variation in adsorption ...

Additionally adsorbed Gas gas amount, moles/g

12 Hydrogen 8 Mitrogen 18 Carbon dioxide Ammonia gas 0.5 Ethylene

When the silica gel is heated to 100°C, its properties return to their initial state, i.e. annealing occurs. The increase in adsorption power remains practically constant at room temperature. The lower the temperature (down to -150°C), the more rapid the adsorption process. The adsorption power of silica gel increases with decreasing temperature, but the increase is greater during gamma irradiation. Results are explained as follows: (1) The hydroxyl group is destroyed by irradiation, and free valences are formed; (2) electrically charged active centers are formed; (3) the bonds between free radicals are ruptured. A. N. Terenin et al. (DAN SSSR, 66, 885, 1949) are mentioned. There are 3 figures, 1 table, and 6 references: 5 Soviet and 1 non-Soviet.

Card 2/3

33100

S/638/61/001/000/025/056 B104/B138

Variation in adsorption ...

ASSOCIATION: Fiziko-tekhnicheskiy institut AN UzSSR (Physicotechnical Institute AS Uzbekskaya SSR)

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Card 3/3

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s/166/50/000/006/008/008 C111/C222

AUTHORS: Ablyayev, Sh.A., Yermatov, S.Ye. and Starodubtsev, S.V., Academician of the Academy of Sciences Uzbekskaya SSR.

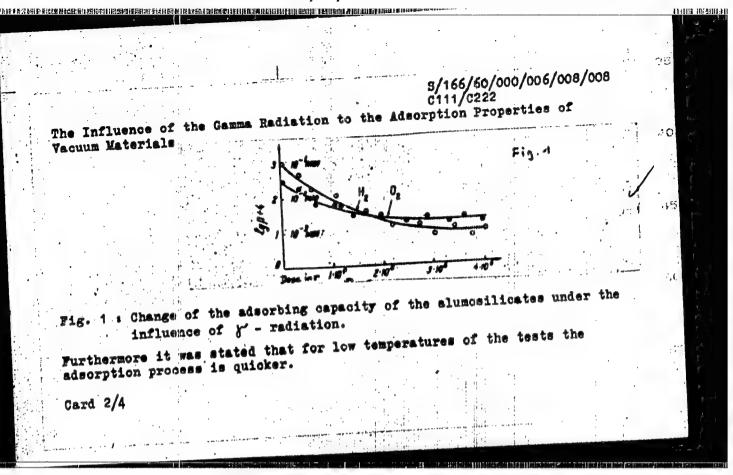
TITLE: The Influence of the Gamma Radiation to the Adsorption Properties of Vacuum Materials

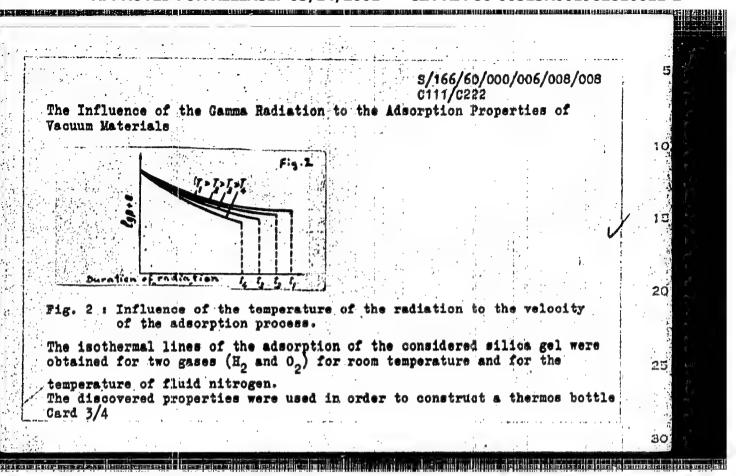
PERIODICAL: Isvestiya Akademii nauk Uzbekskoy SSR, Seriya fizikomatematicheskikh nauk, 1960, No. 6, pp. 95 - 95

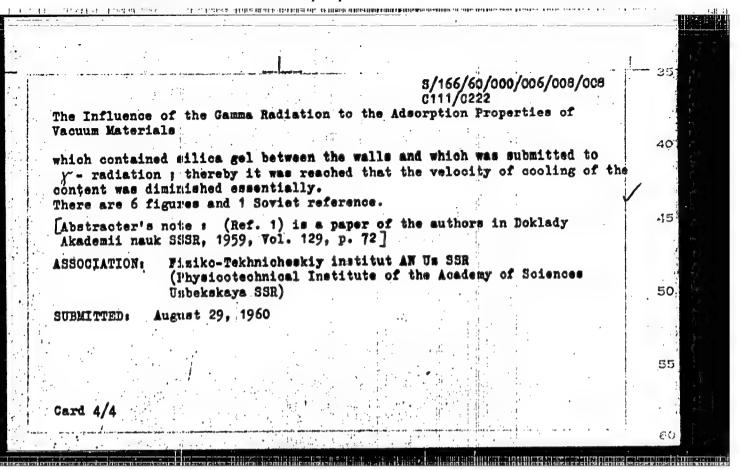
TEXT: In (Ref. 1) the authors showed that the adsorption properties of silica gel are changed essentially by Y - rays Co⁶⁰. The present paper is a continuation of (Ref. 1). The authors investigate the adsorption properties of the types K(K(KSK) and ACM(ASM) of the silica gel properties of the types K(K(KSK) and ACM(ASM) of the silica gel and of the alumosilicates. It was stated that the adsorbing capacity of the alumosilicates after a Y - radiation increases somewhat and the adsorbing capacity of the silica gel increases strongly.

Card 1/ 4

30







YERMATOV, S., CAND PHYS-MATH SCI, "CHANGES IN THE ADSORP-TION PROPERTIES OF SILICA GEL UNDER RECENTED GAMMA-RAYS."

TASHKENT, 1961. (ACAD SCI UZSSR. PHYS-TECH INSTITUTE).

(KL-DV, 11-61, 208).

-10-

8/844/62/000/000/119/129 D207/D307

AUTHORS: Starodubtsev, S. V., Ablyayev, Sh. A., Vasil'yeva, Ye. K.

and Yermatov, S. Ye.

TITLE: Effect of p radiation on adsorption properties of silica

gels

SOURCE: Trudy II Vsesoyuznogo soveshchaniy po radiatsionnoy khi-

mii. Ed. by L. S. Polak. Moscow, Izd-vo AN SSSR, 1962,

689-692

TEXT: Factory-made silica gel of KCK (KSK) grade was heat-treated in evacuated ampoules and then subjected to 7 rays at dose rates up to 340,000 r/hour. Adsorption was then investigated by admitting a gas or vapor to the ampoules held at temperatures from +20°C to liquid-nitrogen temperature. On cooling, the adsorption ability of silica gel increased even without irradiation, but 7 rays intensified this increase. The amount of oxygen adsorbed rose linearly with pressure of the admitted gas or vapor in unirradiated and irradiated silica gel, indicating the same nature of adsorption cen-

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Effects of) radiation ...

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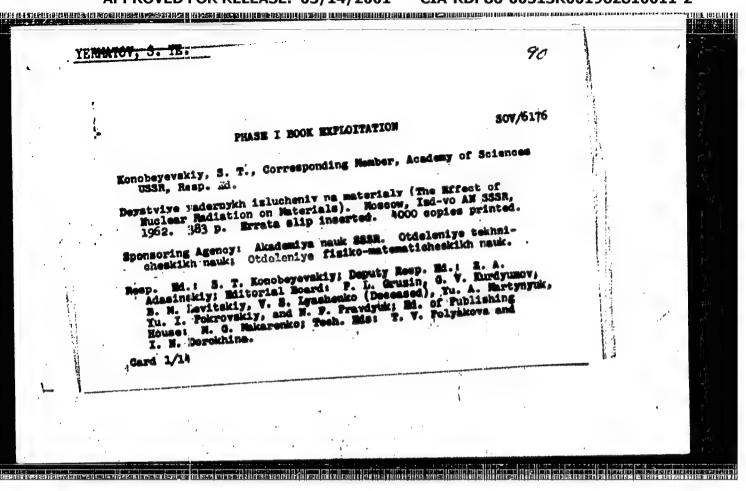
ters in both cases. The silica gel surface became saturated with adsorption centers at doses of $2-3 \times 10^6$ r. Gamma irradiation raised the amount of heptane vapor that could be adsorbed on silica gel (this effect was smaller than for the majority of gases) but made no difference to the adsorption of benzene vapor. Irradiation of aqueous solutions of ammines of the $[\text{Co(NH}_3)_6]\text{Cl}_3$ type in direct contact

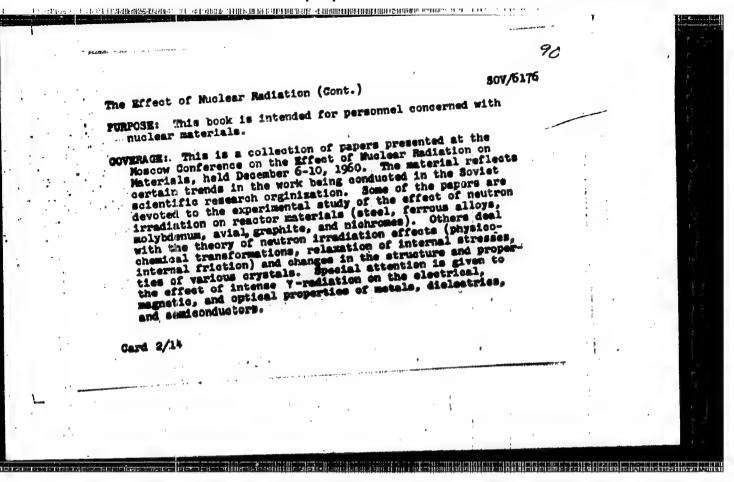
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with silica gel raised the amount of liquid adsorbed because of radiation-induced chemical reactions in the solutions rather than due to changes on the silica gel surface. Gamma-irradiation raised also the amounts of oxygen and hydrogen that could be adsorbed by aluminosilica gel. A practical application of these observations consisted of placing practivated silica gel between the walls of a thermos flask. This improved the vacuum between these walls, by adsorbing more gas than unirradiated silica gel, and thus reduced heat transmision through the walls. Such thermos flasks were prepared at the Ashkhabadskiy stekol nyy kombinat im. V. I. Lenina (Ashkhabad Glass Combine im. V. I. Lenin). There are 7 figures.

ASSOCIATION: Fiziko-tekhnicheskiy institut AN UzbSSR (Physico-Technical Institute AS UzSSR)

Card 2/2





| | The Effect of Muclear Radiation (Cont.) | W/6176 | |
|---|---|--|--|
| • | Starodubteev, S. V., in. M. Usmanova, and V. M. Mikhaelyan. Change in Gertain Electrical Properties of Boron and Amorpho Selenium Under the Action of y-Irradiation | 355 . | |
| | Starodubtsev, S. V., and Sh. A. Vakhidov, Luminescence of Crystalline (marts Subjected to UV- and Y-Nays | 362 | |
| | Starodubtsev, S. V., Sh. A. Ablyarev, and S. Ye. Yernatov. Effect of Y-Ray Flux on Absorption Properties of Vacuum Materials Change in absorptive properties of various silica gels and alumosilicates, subjected to Y-ray doses of 150,000 to 350,000 r/h, were investigated. | 366 | |
| | Trinkler, E. I. Effect of Y-Irradiation on Fermoability of Some Ferrites | 370 | |
| | Strel'nikov. P. I., A. I. Fedoranko, and A. F. Klyncharev. Effect of Froton Irradiation on Merchardness of Iron and Steel | 374 | |
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ACCESSION NR: AT3007248

- S/2952/63/000/000/0011/0018

AUTHORS: Starodubtsev, E.S. V.; Ablyayev, Sh.A.; Yermatov, S.Ye; Pulatov, U.U.

TITLE: Changes in adsorptivities of silicagels and zeolites under the action of high-frequency discharges

SOURCE: Radiatsion. effekty* v tverd. telakh. Tashkent, Izd-vo AN UzbSSR, 1963, 11-18

TOPIC TAGS: adsorption, adsorptivity, silicagel, zeolite, electric discharge, slow electron, gamma ray, cosmic radiation, temperature effect, isotherm, high-frequency discharge

ABSTRACT: The paper reports the basic results of an experimental investigation of the effect of fluxes of slow electrons on the adsorption properties of synthetic zeolites and silicagels. Test objects were: Silicagel Mark KSK and synthetic zeolites of the types 4% (NaA) Gor'kovskoye, CaA 5% Gor'kovskoye, 13x(Nax) Gor'kovskoye, 4% (NaA) Groznoye, and CaA 5% Groznoye. High-frequency electric discharges served as slow-electron sources. The changes in the adsorptional properties were investigated experimentally by the adsorption of gases by adsorbents measured by manometric tubes. The specimen adsorbent, contained in a glass ampoule (A), is

Card 1/3

ACCESSION NR: AT3007248

first heated to 350-400°C under continuous evacuation. The A is then filled with . the test gas from a reservoir V, following the evacuation of the air from the entire system down to 10⁻³ to 10⁻⁴ mm Hg. The gas is permitted to enter the adsorbent container A up to a specified pressure, whereupon A is soldered tight and thus cut off from the vacuum equipment and held at room temperature until the establishment of an equilibrium pressure, which is of the order of 10" mm Hg. The instrument is then exposed to the action of the high-frequency discharges. Zeolites: Test results, plotted in the form of curves, show that all types of zeolites gain in adsorptional capacity under the effect of slow electrons. These changes increase with increasing irradiation time up to a specified limit and then achieve saturation. after about 6 to 10 min. Optimal results were obtained with the Gor'kovskoye zeolites of the types 13x(Nax) and CaA 5A. Isotherms of ordinary and induced adsorption of zeolites with reference to dry air at temperatures of 20 and -196°C were derived. Silicagels: Exposure to the discharges increased the adsorptivity of silicagel substantially. Saturation at any given oscillatory power was achieved after 8-15 minutes. Isotherms of ordinary and induced adsorption of silicagel with respect to dry air in the 10-1 to 10-3-mm-Hg range were obtained at temperatures of 0, +30, +60, and -196°C. Adsorbent temperature exerted a noticeable effect on the magnitude of both ordinary and induced adsorption. The adsorptivity of silicagel and zeolites increases with decreasing temperatures even without irradiation.

Card 2/3

THE MESTAL PHONE REPORTED THE TRANSPORTED TO WISHINGTON IN THE WINNESS OF THE PROPERTY OF THE ACCESSION NR: AT3007248 However, the changes are substantially greater under irradiation, and the adsorption is much more parmanent. The effect of lower temperatures is stronger on zeolites than on silicagels. Some light is shed on the effect of slow electrons and gamma-ray radiational effects on the surface layer and into the depth of an adsorbent. Orig. art. has: 7 figures. ASSOCIATION: none ENCL: 00 DATE ACQ: 140ct63 00 % SUBMITTED: OTHER: 000 NO REF SOV: PH-EE, MA SUB CODE: Card

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\$/2952/63/000/000/0019/0021

ACCESSION NR: AT3007249

AUTHORS: Starodubtsev, S. V.; Ablyayev, Sh. A.; Yermatoy, S. Ye; Azizov, S. A.

TITLE: Effect of gamma radiation on the adsorptional properties of synthetic zeolites,

SOURCE: Radiatsion. effekty* v tverd. telakh. Tashkent, Izd-vo AN UabSSR, 1963, Saa

19-21

TOPIC TAGS: adsorption, ordinary adsorption, supplementary adsorption, radiation-induced adsorption, zeolite, gamma ray, gamma-ray-induced adsorption, radiation; gamma radiation, temperature effect, isotherm

ABSTRACT: The paper describes an experimental investigation of the effect of gamma rays on the adsorptivity of synthetic zeolites. The tests were performed by the ordinary volumetric method on 3 Gor'kovskoye specimens of the types 4A (NaA), CaA 5A, and 13x (Nax), and two Groznoye specimens 4A (NaA) and CaA 5A. The zeolite specimens were first heat-treated thoroughly at temperatures of 350-400°C at pressures between 10-1 and 10-6 mm Hg for several hours. The zeolites were then exposed to gamma rays of a radiation dosage rate of 150 to 350,000 r/hr, with a total dose of 2 to 3.100 r. The adsorptivity of the zeolites was found to be

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ACCESSION NR: AT3007249

significantly increased; the increase grew to a certain limit depending on the intensity of the radiation dose. The effect of the glass on the test results was determined by identical control ampoules with O and H, with and without adsorbents, exposed to gamma radiation. It was found that the ampoules not containing adsorbents maintained a constant gas pressure. Therefore, the effect of the glass was found to be nil. It was found that the adsorption temperature affects the magnitude of the gamma-ray effect substantially. The radiational effect decreases at elevated temperatures, that is, a radiational anneal occurs. The effect disappears completely at 300-400°C. It is noted that following an anneal the limiting pressure occurs at lower values of the radiational dose. Comparative isotherms of supplementary and ordinary adsorption of an irradiated zeolite were plotted for dry air at -196° and at room temperature. The nature of the radiation effect observed is explained by the knocking out of a Compton electron by a primary gamma quantum, whereupon the fast electrons pass along a path of 2-3 mm within the zeolite. Having expended their energy on the ionization of the matter, they form a large number of relatively slow electrons with energies of the order of tens of ev. The resulting strong ionization forms negative and positive ions which produce excitaitions and other defects of various kind. The number of possible defects per gamma quantum ordinarily amounts to several tens of thousands; these defects do not differ from those obtainable by UV and X-ray impingement. The supplementary

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adsorption of gases on the zeolites occurs in such defects. Orig. art. has: 3 figs.

ASSOCIATION: none

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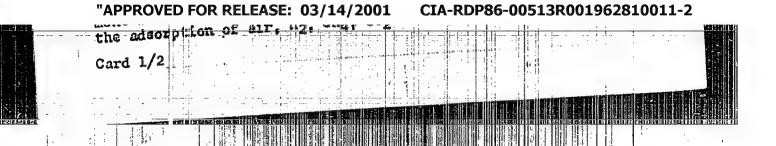
SUB CODE: MA, PA, EE, CH NO REF SOV: 005 OTHER: 000

S/109/63/006/002/019/028
D413/D308

Starodubtsev, S.V., Ablyayev, St.A., Yermatov, S.Ye.
and Pulatov, U.

The effect of radio-frequency discharges on the cd.
sorption properties of silica gd.
sorption properties of silica gd.
PERIODICAL: Radiotekhnika i electronika, v. 8, no 2, 1963,
328-330

The authors have earlier (Dokl. AN SSSR, v. 129, no. 6, 1960, nault. no.



The effect of radio-frequency ...

8/109/55/008/002/019/028 D413/D503

times was measured by manameter tubes. The resulting curves show increases it adsorption closely similar to those obtained by the action of Y-radiation, ranging from zero for He to a saturation value of 0.4 \$\mu\$ mole g-1 for H2. The induced adsorption disappears completely in baking at 350°C. Isotherns are also given for the induced adsorption of dry air at 0° 30° and 60°C over the range

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STARODUBTSEV, S.V., akademik; ABLYAYEV, Sh.A.; YERMATOV, S.Ye.; PULATOV, U.U.

LECTION TO THE POST OF THE POS

Charge in the adsorbing capacity of silica gel induced by high-frequency discharges. Izv. AN Uz. SSR. Ser. fiz.-mat. nauk no.6:77-78 '61. (MIRA 16:12)

1. Fiziko-tekhnicheskiy institut AN UzSSR. 2. Akademiya nauk UzSSR (for Starodubtsev).

فيسور وأرثابها ID/GO/GE LIP(c) L 2142-66 ENT(m)/EPF(c)/EPF(n)-2/ENP(t)/EMP(b) UR/0000/62/000/000/0366/0369 ACCESSION NR: ANSO23820 B Staredubtsev, S. V.; Ablyayev, Sh. A.; Yersetov, S. Ye. TITLE: Effect of gamma fluxes on the adsorptive properties of vacuum materials SOURCE: Sovembehaniye po probleme Devetvive vadernyth inlantenty na materialy.

Moscow, 1960. Devetvive yadernyth isluchenty na materialy (The offect of nuclear radiation on materials); doklady soveshchaniya. Hoscow, Ind-vo AN SSSR, 1962, TOPIC TAGS: eilica gel, aluminum silicatu, gamma irradiation, irradiation effect, ABSTRACT: The article continues the study of K-ray-induced changes in the adsorptive properties of KSK and ASH silica geldend plant-produced aluminosilicates. Oxygen and hydrogen were used as the adsorbed gases, and the radiation dose rate was (150-350) 103 r/hr. All the results showed an increase in adsorptive capacity that was much more pronounced in silica gels than in aluminosilicates. The temperature dependence of this redistion effect was investigated between +100 and -1300, and the adsorptive capacity was found to increase with decreasing temperature (this increase was much greater than that of nonigradiated samples). The adsorption isotherms were found to be linear both at room temperature and at the

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ACC NRI AP7004640

SOURCE CODE: UR/0288/66/000/003/0104/0105

AUTHOR: Umarov, G. Ya.; Lyutovich, A. S.; Yermatov, S. Ye.; Karimov, F. R.

ORG: Physico-technical Institute, AN UzSSR, Tashkent (Fiziko-tekhnicheskiy institut AN UzSSR)

TITLE: The possibility of obtaining semiconductor and difficultly fusible materials with the aid of a jet discharge

SOURCE: AN SSSR. Sibirskoye otdeleniye. Izvestiya. Seriya tekhnicheskikh mauk, no. 3, 1966, 104-105

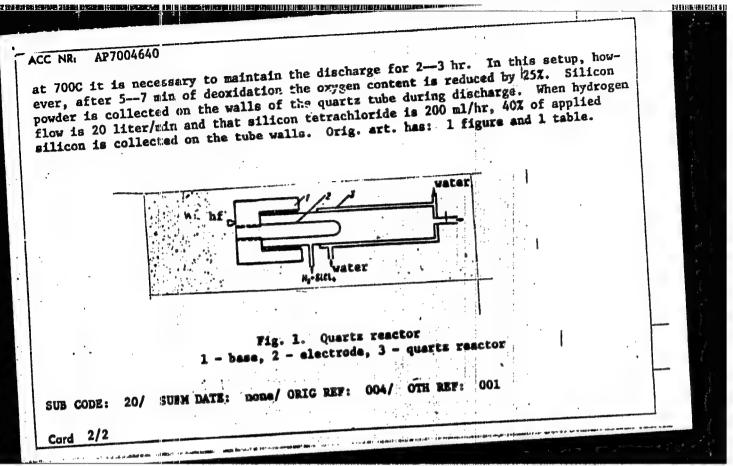
TOPIC TAGS: thermal reactor, oxidation reduction reaction, gas discharge, high frequency discharge, metal apide, weln could nuclear metal

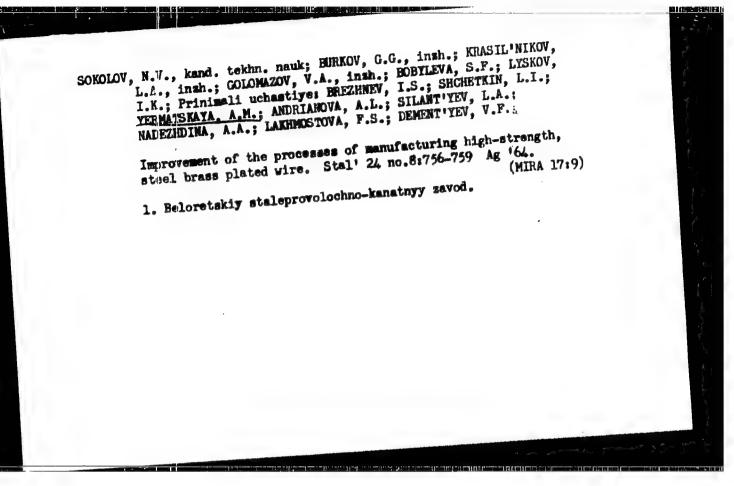
ABSTRACT: A gas discharge setup (see Fig. 1) is described for deoxidizing such materials as silicon oxide and metallic oxides. The discharge in this water-cooled quartz reactor is maintained by 10-kw, 25-Mc, rf energy source and the raw materials are SiCl₄ and M₀O₃. The reactor is 75 cm long and 20 cm in diameter. When molybden-

um oxide is being reduced cooling is not necessary. The discharge is started at silicon electrode progressing to the surrounding mixture of hydrogen and silicon tetrachloride. When molybdenum oxide is being reduced the electrode is made of molybdenum. Under normal conditions to reduce molybdenum trioxide to dioxide state

Card 1/2

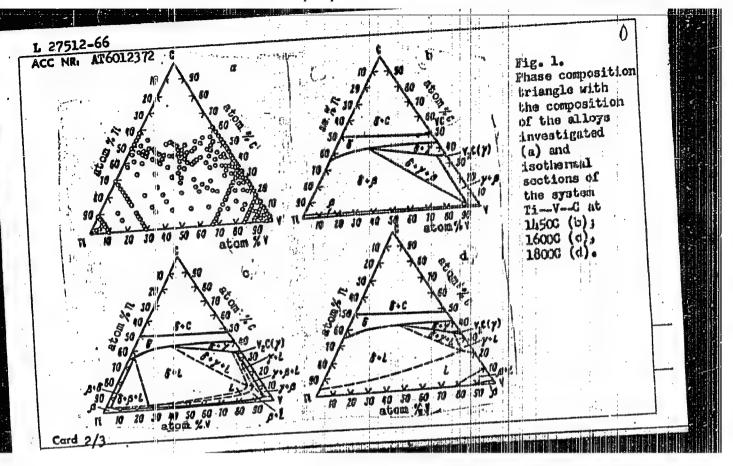
UDC: 621.315.592+669.018.45+669.094.1





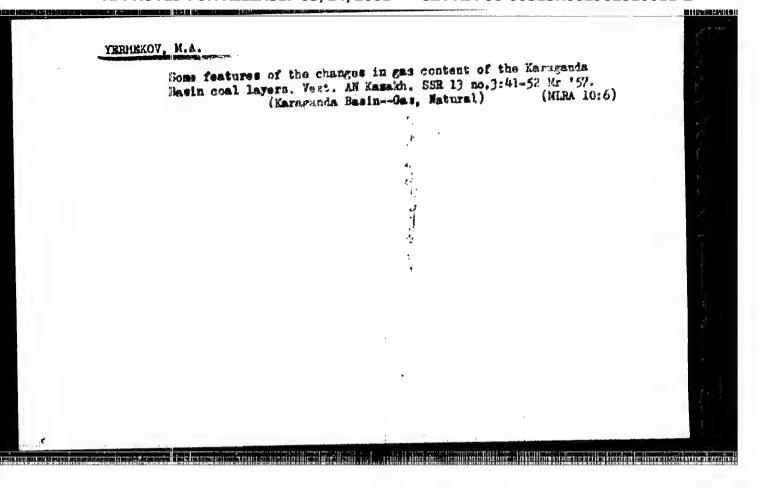
| ACC NRI | 56 EWT(n)/T/ AT6012372 Tret'yachenko, | * * | | /G8 Ba UR/OOCO/65/0 | 55/000/0075/0081 H (3/1 | |
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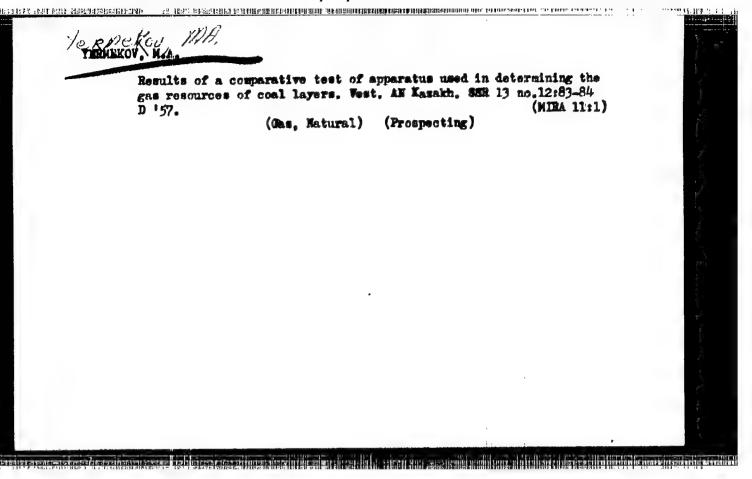
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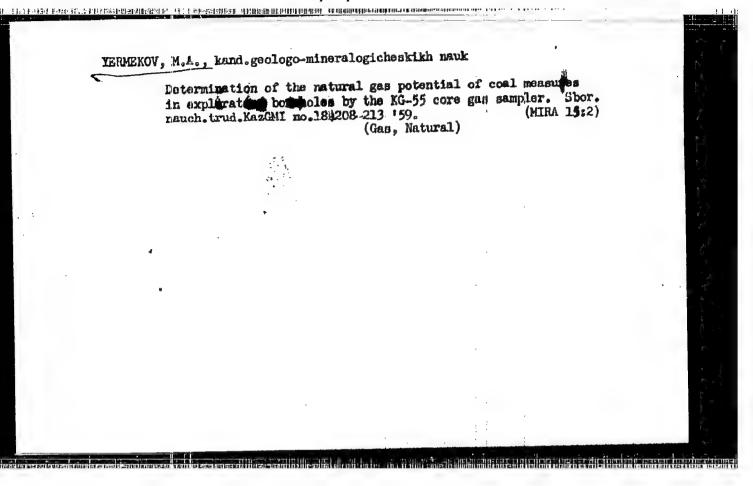


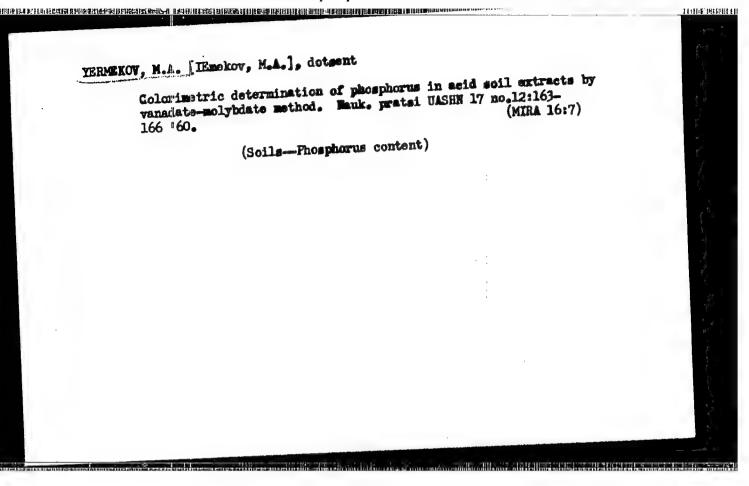


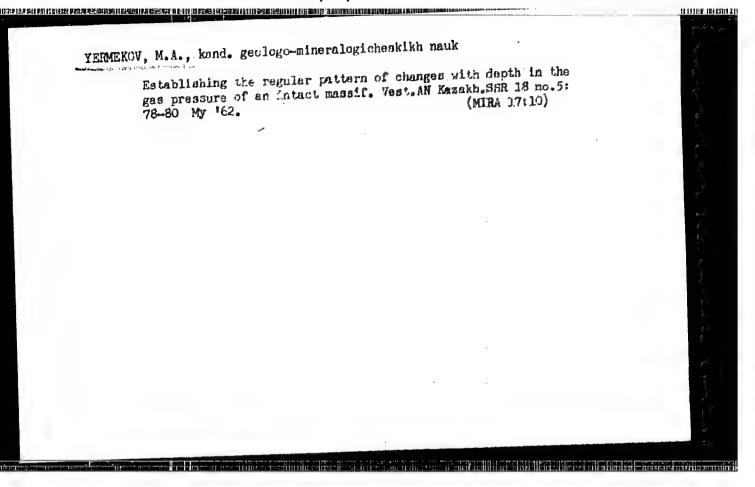
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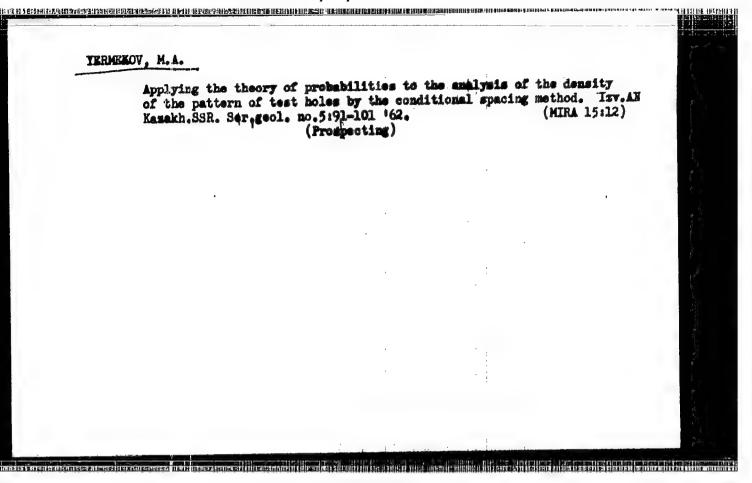
Studying the gas-kernel of the coal-bearing deposits of Karaganda basin in the process of geological prospecting and Alma-Ata, 1958. 12 pp (Min of Higher Education USSR, Kazakh Mining and Metallurgical Inst), 150 copies (KL, 35-58, 106)

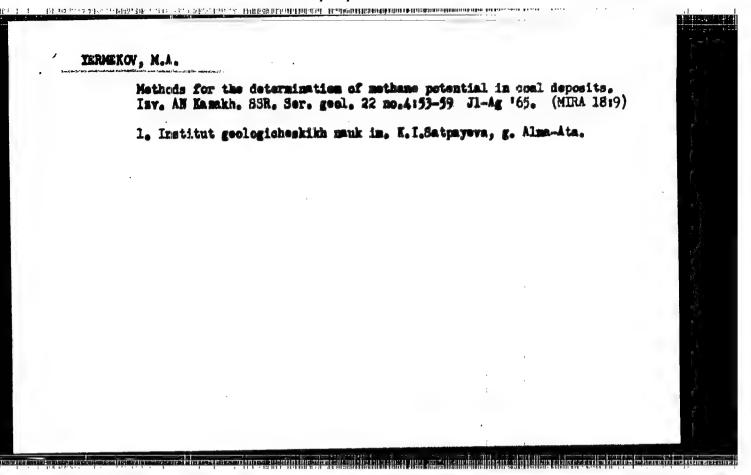
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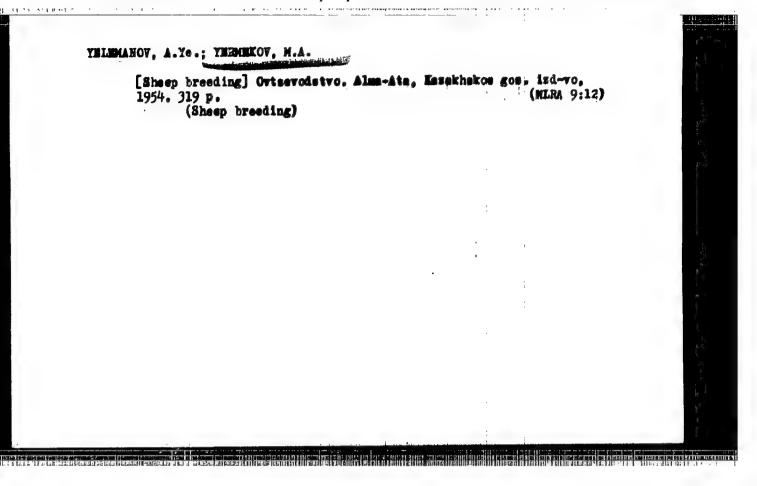












YERMEKOV, N.A. (Alma-Ata); GLADKOV, P.F. (Alma-Ata)

Vitality and adaptability of animals. Agrobiologiia no.4:584-587

Jl-Ag *62. (MIRA 15:9)

(KAZAKHSTAN-SHEEP BREEDING)

YERMEKOV, M.A., zasluzhennyy deyatel nauki Kazakhskoy SSR; GLADKOV, P.F., mladshiy nauchnyy sotrudnik; CHUMIN, N.P., mladshiy nauchnyy sotrudnik

Fat-tailed sheep of central Zazakhstan. Zhivotnovodstvo 24 no.9:61-67 S 162. (MIRA-15:12)

1. Kazakhskiy nauchno-issledovatel'skiy institut zhivotnovodstwa. (Kazakhstan-Sheep breeds)

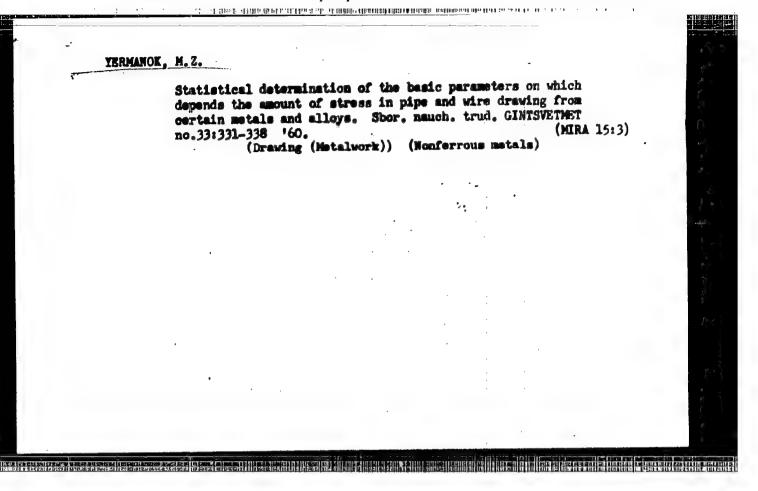
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S/136/60/000/012/009/010 E193/E183

Investigation of Stresses During Extrusion of Ribbed Aluminium Alloy Components

between the calculated and factual magnitude of P was only 21%. The general conclusion reached was that if the magnitude of $S_{\rm d.c}$ and $K_{\rm kp}$ for a given alloy is determined experimentally, the extrusion pressure can be calculated with sufficient accuracy with the aid of formula (la). There are 5 figures, 4 tables and 8 Soviet references.

Card 7/7



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31741 \$/136/61/000/012/005/006 \$193/\$383

AUTHORS:

Dontsov, S.N., Yermanok, M.Z., Candidates of Technical Sciences and Chizhov, I.N., Engineer

TITLE:

Strength characteristics of titanium alloys and their application in calculating stresses during plastic-

than a first of the trade of the residence of the second o

working operations

PERIODICAL: Tswetnyye metally, no. 12, 1961, 74 - 76

TEXT: Lack of experimental data on the resistance of Ti alloys to deformation at various temperatures and deformation rates causes difficulties in designing equipment for plastic—working of these materials and in establishing optimum working schedules. Hence the present investigation, which is concerned with the properties of pure Ti (BT| (VT1)) and Ti alloys (BT6 (VT6), BT5 (VT5) and OT4). In Fig. 1, the hot tensile strength (σ_B , kg/mm²) of these materials is plotted against temperature (°C). It will be seen that at 1 050 - 1 150 °C, i.e. in the hot-working temperature range, σ_B of all four materials is very much the same. These values, however, cannot Card 1/5/

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Strength characteristics of

be used as the basis for calculating stresses during hotworking operations because they represent strongth of undeformed material, whereas the strength of an alloy near the exit end of the deformation region depends on the deformation (rolling) rate. The effect of strain rate on $\sigma_{\mathbf{R}}^c$ of the alloys studied is illustrated in Fig. 2, where of of the alloy VT5 is plotted against test temperature (°C), curves 1-4 relating, respectively, to strain rates of 0.33, 280, 740 and 1 120 %/sec; (similar results were obtained for the alloy VT6). The data presented in Fig. 2 are reproduced in a different manner in Fig. 3, where the so-called strengthming coefficient (c) is plotted against the strain rate (N, %/sec) at temperatures indicated by each curve. If it is assumed that the average resistance of a metal $S_{\Omega,Cp}$, is an arithmetical mean to deformation during rolling. of its tensile strength near the entry and exit ends of the deformation region, it can be calculated from the formula:

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Strength characteristics of

$$S_{A,CP} = \frac{1+c}{2} \cdot \sigma_{5} \tag{2}$$

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where of is the tensile strength determined by the CTOT static test at a given temperature and c is the strengthening coefficient corresponding to a given rolling temperature and speed. If, as has been postulated by Perlin, of is a geometrical means of of near the exit and entry ends of the deformation region, Eq. (2) becomes:

$$S_{A,CP} = S_{ETST} \cdot \sqrt{c}$$
 (3).

The magnitude of c is independent of the rate of deformation in cold-rolling and the average resistance to deformation in this case is simply Card 3/5/

s/136/61/000/012/005/006 E193/E383

Strength characteristics of

the arithmetical mean of UTS of the alloy before and after rolling. A more accurate value of Space in cold-rolling is given by the formula proposed by M.Z. Yermanok in Ref. 5 (IVUZ, Tsvetnaya metallurgiya, 1959, no. 6):

$$S_{\text{A},ep} = \frac{g_{\text{Hay}} \cdot g_{\text{Koh}}}{g_{\text{Hay}} \cdot g_{\text{Koh}}}$$
(5)

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where 5 and 5 denote, respectively, the UTS of the 5H34 5KOH alloy before and after rolling,

FH34 and F denoting the cross-sectional area of the stock at the entry and exit ends of the deformation region.

Card 4/84

CIA-RDP86-00513R001962810011-2 "APPROVED FOR RELEASE: 03/20/2001 E RESTAURANT MINIMER HALL THE PROPERTY OF THE 5/136/62/000/002/002/004 33165 E073/E135 Zlotin, L.B., and Yermanok, M.Z. 4016 Diagrams for calculating the dependence of the resistance to deformation on the duration and degree 10.7200 AUTHORS: PERIODICAL: Tsvetnyye metally, no.2, 1962, 66-69 A basic parameter for calculating the forces required TITLE: TEAT:

In metal forming is the resistance to deformation Sd;

which is a second forming in the deformation of the deformation greatly influenced by the degree and duration of the deformation. Experimental investigation of these factors is very difficult; also, no standard high-speed experimental equipment is in existence. Therefore various authors attempted to derive formulae for analytical determination of the resistance to deformation during high speed deformation. In all these formulae the decisive parameter is the speed of the relative deformation is the relative deformation in fractions of unity, where ô Card 1/4

33165

Diagrams for calculating the ...

Card 2/4

S/136/62/000/002/002/00⁴ E073/E135

However, the is the duration of the deformation in seconds. speed of deformation is not a universal parameter; also, the effects of the degree of deformation and the duration of deformation on Sd are not identical. Published data and results obtained by the authors indicate that the influence of the degree of deformation is high, and that it is advisable to take into consideration separately the influence of the degree and the duration of the deformation. The present authors derived a mathematical expression for the influence of the degree and duration of the deformation based on extensive experimental results obtained on the most widely used heavy nonferrous metals and alloys under a great variety of conditions. The Sd versus relations are represented in the form of curves which converge into a single point denoted as the initial resistance to which is the ultimate deformation at the given temperature Sd.H strength ob determined from static tests. This assumption is based on the following considerations: 1) The yield point does not characterise the resistance to deformation if the deformation

CIA-RDP86-00513R001962810011-2" APPROVED FOR RELEASE: 03/20/2001

33165

Diagrams for calculating the ... S/136/62/000/002/002/004 E073/E135

is predominantly plastic; the force required for plastic stretching or compression is more relevant from this point of view. 2) The real stresses during plastic extension are approximately equal to the strength value and, therefore, it is advisable to use this value as an initial characteristic in the calculations. The authors derived an empirical relation by mathematical statistics methods, using the method of least squares, for determining the coefficients of the sought equation, which is:

$$S_{d,K} = S_{d,H} \cdot a \cdot e^{-b \cdot lg \cdot \tau}$$
 (2)

where a and b are coefficients which depend on the nature of the material, the temperature and degree of deformation. This equation can be transformed into:

$$lg \frac{S}{S} \frac{d.K}{d.H} = A - B lg \tau$$
 (3a)

Card 3/4

Diagrams for calculating the ...

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In the coordinates $\lg \frac{S_{d,K}}{S_{d,k}} - \lg \tau$, Eq.(3a) can be represented

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in the form of straight lines, and from this equation diagrams were plotted which converge into a point and permit the determination of $S_{d,K}$. The results are in good agreement with

experiment, the maximum divergence being less than 15%. Analysis of the diagrams plotted in the paper indicates that Eq.(2) reflects the non-identity of the influence of the degree and duration of deformation on the value of S_d . The proposed method was verified by comparison with published experimental results and the agreement was found to be satisfactory. The S_d versus a diagrams reduce considerably the amount of work involved in calculating the value S_d which is required for force calculation in metal forming processes.

There are 3 figures, 1 table and 11 Soviet-bloc references.

Card 4/4

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37536 S/136/62/000/005/001/002 E193/E383

1.1310

Yermanok, M.Z. and Shcheglov, G.M.

AUTHORS: TITLE: Extrusion by the inverted and combined method on presses with limited travel of the container

presses with 11m2 35 no. 5, 1962, 61 - 65

PERIODICAL: Tsvetnyye metals, A for fabricating aluminium or TEXT: When extrusion is used for fabricating the container, magnesium—alloy sections without lubricating the container, magnesium—alloy sections without lubricating the container much lower extrusion pressures are required if inverted extrusion much lower extrusion pressures narrows considerably in most of the limited travel (200 - 350 mm) of the container is employed. The limited presses narrows considerably in most of the existing extrusion presses narrows considerably the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the range of applicability of this method. This difficulty, the container of the c

S/136/62/000/005/001/002 Extrusion by the inverted E193/E383

then moved forward by the extrusion ram 1 and pressure disc until it becomes flush with the front end of the container liner, the container itself being moved back against its stop (Fig. 16). The die head is then brought into position and locked, after which the inverted-extrusion operation is carried out (Fig. 16). As a result of the pressure acting on the billet, the container with the billet advances towards the die head, the dis-holder enters the container liner and the metal is extruded through the die. Movement of the container ceases when the entire length of the die-holder has entered the container and this completes the first stage of the operation (Fig. 12). Further extrusion can be done either by the direct or by the inverted method. In the former case, the entire process will have included both direct and inverted extrusion and can, therefore, be referred to as "combined method of extrusion"; the advantages of this method are demonstrated by data reproduced If the reduction of the extrusion pressure attained in Table 1. by using the combined method is not sufficiently large, the operation, after reaching the stage shown in Fig. 11, can be

Card 2/5

Extrusion by the inverted

S/136/62/000/005/001/002 E193/E383

continued by the inverted method, the consecutive singes of which are shown in Fig. 10, e and —. The combined extrusion method was tested by using it to fabricate a most difficult type of extruded section, namely, a section comprising three different profiles, which was extruded with the aid of three split dies. The results indicated that the combined method required an extrusion pressure 625 - 750 tons lower than that required for direct extrusion, which means that both longer billets can be used and smaller cross-section profiles can be made by this method. In addition, the lower temperature of the billet makes it possible to increase the extrusion speed from 0.6-0.7 to 1-1.1 m/min, whereby the efficiency of the process is increased. There are 5 figures and 3 tables.

1

Card 3/5

YERMANOK, M.Z.; SHIPILOVA, L.P.

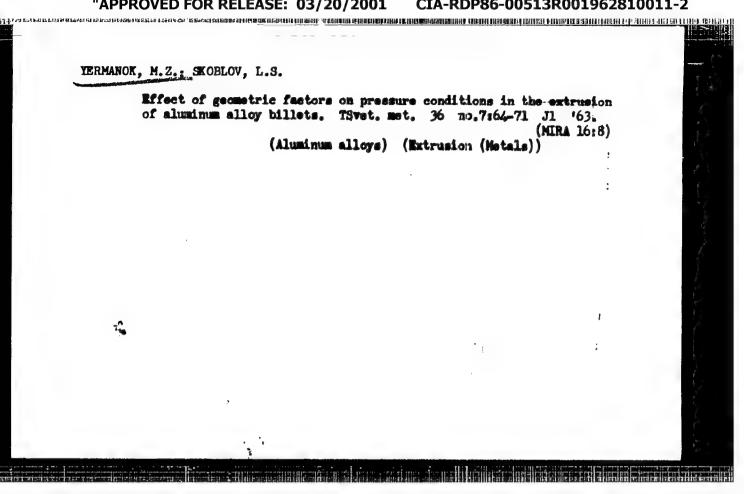
Mechanical properties of semifinished AMg-6 alloy products.

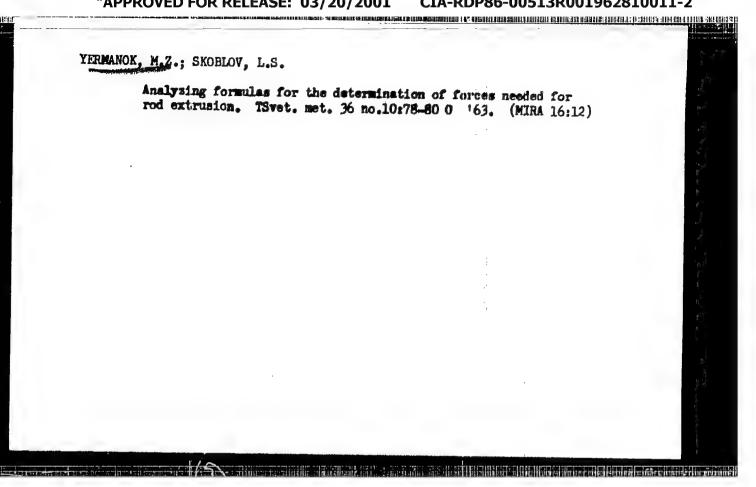
Metalloved. i term. obr. met. no.10:36-37 0 '63. (MIRA 16:10)

ZACHAROV, M.F.; GLEBOV, Yu.P.; YERMAROK, M.Z.

Pressure conditions in the extrusion of pipe with an arbitrary internal shape. Izv. vys. ucheb. zav.; tsvet. met. 6 no.3:128-136

163. (Extrusion (Metals))





CIA-RDP86-00513R001962810011-2" APPROVED FOR RELEASE: 03/20/2001

ACCESSION NR: AP4030670

8/014:9/64/000/004/0043/0044

AUTHOR: Yermanok, M. Z.; Tomashevskaya, I. M.

TITIE: Influence of preliminary cold deformation on mechanical properties of alloy D16 in tempered pipes

SOURCE: Metallovedeniye i termicheskaya obrabotka metallaw, no. 4, 1964, 43-44

TOPIC TAGS: cold rolled pipe, pipe deformation, pipe strungth, Di6 alloy, cold drawn pipe, tempered pipe

ABSTRACT: Thin walled pipes of D16 alloy made by cold rolling or drawing of a hot forged billet show a degree of deformation from 30-35% to 80-85%, resulting in considerably different mechanical properties. Although this is a very important practical problem, its study has been inadequate. The goal of the authors was to determine the mechanical properties of tempered pipes depending on the degree of deformation prior to tempering. As a result of cold rolling an annealed billet into pipes, their annealing and tempering from 500C in vater, the following results were obtained: (1) the wall thickness (1-3 mm) has but little influence on the mechanical properties of D16 alloy pipes; and (2) increasing the rate of cold

Card 1/2

ACCESSION NR: AP4030670

deformation to 70% prior to tempering considerably increases the strength characteristic, and the value of relative elongation corresponds the COST standard 4773-49. Further increase in deformation does not improve the strength characteristic of pipes. Minimum emounts of preliminary deformation required to reach peak levels of the yield point according to COST 4773-49 have been established. Orig. art. has 2 figures, no formulas, no tables.

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SUB CODE: MM NO MET SOV: 000 OTHER: 000

Card 2/2

ACCESSION NR: AP4015111

Card 1/8 2

3/0136/64/000/002/0062/0065

AUTHOR: Perlin, I.L.; Glebov, Yu.P.; Yermanok, M.Z.

TITLE: Effect of temperature, degree and rate of deformation on the

deformation strength of aluminum alloys.

SOURCE: Tsvetny ye metally No.2, 1964, 62-65

TOPIC TAGS: aluminum alloy, D:6 aluminum alloy, V95 aluminum alloy, AD31 aluminum alloy, deformation strength, deformation rate, deformation temperature, deformation strength temperature function

ABSTRACT: The effect of different temperatures (360, 420, 4800) and various deformation rates (0.19, 0.8, 220 and 880 mm/sec) on the deformation strength S was investigated for D16, V95, and AD31 aluminum alloys. The deformation rate w affects S ; and with increased degree of deformation \(\psi\), the intensity of the growth of S is decreased and in some cases even lowered (for AD31 S is lower at a rate of 14 sec. -/ than at 4 sec. -/). The curves which show the dependence of S on degree of deformation have a maximum, and it is also shown that

ACCESSION NR: AP4015111

the degree of deformation depends on temperature and rate of deformation. As temperature increases the maximum on the curve is shifted in the direction of smaller deformation values; and with increasing rate of deformation, it is shifted in the direction of larger deformation values. Working diagrams (fig.!) of the $S_{\downarrow} = f(t^*)$ relationship were constructed by extrapolation from experimental data for the 3 probable deformation periods encountered in extruding the given alloys. The lower curves $S_{\downarrow\downarrow}$ show the initial values corresponding to S_{\downarrow} for has: 3 figures

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ASSOCIATION: None

SUB CODE: ML

DATE ACQ: 12Mar64

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OTHER: 003

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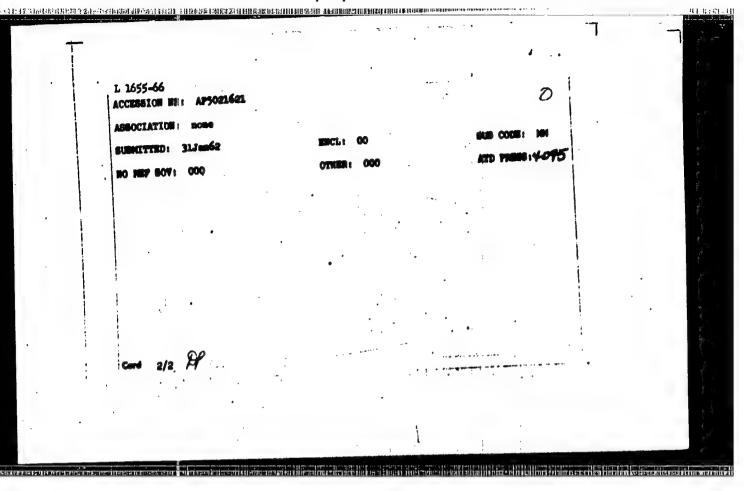
NOSAL', V.V., prof., doktor tekhn.nauk; VERDEREVSKIY, V.A., kand.tekhn.nauk; YERMANOK, M.Z., kard.tekhn.nauk

Review of a book by Z.A.Koffa and others "Cold rolling of pipe." Stal' 24 no.6:536-537 Je '64. (MIRA 17:9)

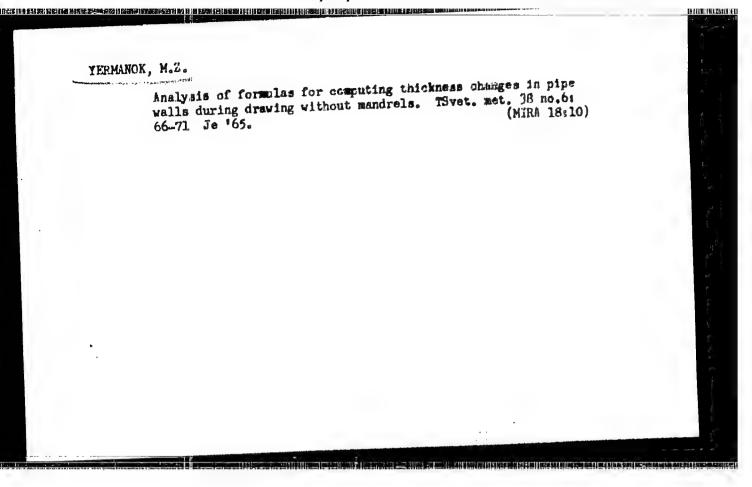
l. Vsesoyuznyy nauchno-issledovatel'skiy i proyektno-konstruktorskiy institut metallurgicheskogo mashinostroyeniya (for Nosal', Verderevskiy).

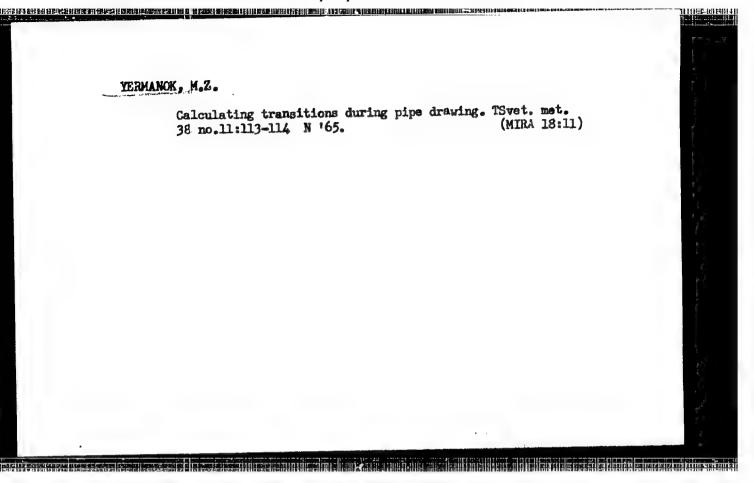
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| | Author Mild's Bounday Gift's Abburtahin, NFAS' Evitaitakiy | A. J.; yv. | |
| I | Rodioney, A. B. W.S. | | |
| | TITLE: Nothed for tube estruction Class by, No. 172601 | | 1 |
| | SOURCE: Byullaten' imbrotoniy i tovernyth meshov, so. 13, 1965, | 101 | |
| | TOPIC TACS: metal, metal tube, metal extrusion, tube extrusion | | |
| | ADSTRACT: This Author Cortificate introduces a suthed for take or | Armion from | |
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| L 1655-66 ENT(d)/ENT(m)/ENP(v)/ENP(k)/ENP(h)/ENP(h)/ENP(h)/ENP(h)/ENP(h)/EMA(d) JD/EN ACCESSION NR: AP5021621 UN/0266/65/000/013/0102/0102 621.979.968.002.58 AUTHOR: Ebofman, L. A.; Godymin, Yu. Yu.; Ronkhov, V. M.; Starikov, V. M.; Kryuchkov, M. M.; Pavrdov, G. VF *Akhmatshin, M. M.; Rvitaitshiy, A. M.; gv.; Noccilabliya A. A.; Paygin, V. I.; Yegorov, I. V.; Roytbarg, L. Km.; Israedk, M. E.; Rodionov, A. B.; Vy.; TITLE: Tool for extrading of tubes. Class 49, No. 172602 SOURCE: Byulleten' isobreteniy i tovarnyth snakov, no. 13, 1965, 102 TOPIC TAKE: tube, metal tube, tube extrusion, extrusion tool, extrusion press W. ABSTRACT: This Author Certificate introduces a tool for the extrasion of tubes from solid ingots, i.e., container, mendrel, veiding chamber, and die. In order to insolid ingots, i.e., container, mendrel, veiding chamber, and die. In order to increase the rigidity of individual tools and ensure their precise position in relation to one another, thereby improving the accuracy of the extruded tubes, the mandrel is to one another, thereby improving the accuracy of the extruded tubes, the mandrel is rigidly mounted in relation to the container; it carries an internal die and is provided with a central compartment for the ingot. Radial canals connect this comvided with a central compartment for the ingot. Radial canals connect this compartment: with the welding chamber, which is formed between container wall and the mandrel surface. [AE] | |
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| | L 5192-66 EWP(-)/EWT(m)/EFF(c)/EWP(t)/T/EWP(t)/EWF(b)/EWA(h) JD/WW/DJ/WH ACC NR: AP5024999 SOURCE CODE: UR/0286/6 W/OOC/D16/0062/0062 | |
|--------------------------------|--|---|
| - | AUTHORS: Uvarov, V. Ya.; Glebov, Yu. P.; Zhuravlev, F. V.; Sukhanova, M. Z.; Rubin, Yu. L.; Zakharov, M. F.; Kochnova, G. P.; Sukhanova, M. P. | |
| | ORG: none | |
| the state of the factor of the | TITLE: Lubricant for heat treatment of metals. Class 23, No. 173869 (announced by the Organization of Mosgorsovnarkhoz (Organizatsiya mosgorsovnarkhoza) | |
| | SOURCE: Byulleten izobreteniy i tovarnykh znakov, no. 16, 1965, 52 | - |
| | TOPIC TAGS: lubricant, metal heat treatment, mineral oil | |
| April On the district of the | ABSTRACT: This Author Certificate presents a mineral oil and graphite lubricant for heat treatment of metals. To prevent metals from sticking to the instrument, talcum and red lead are added to the lubricant. The talcum constitutes 10% by weight of the additive, and the red lead constitutes 8-25% by weight. | |
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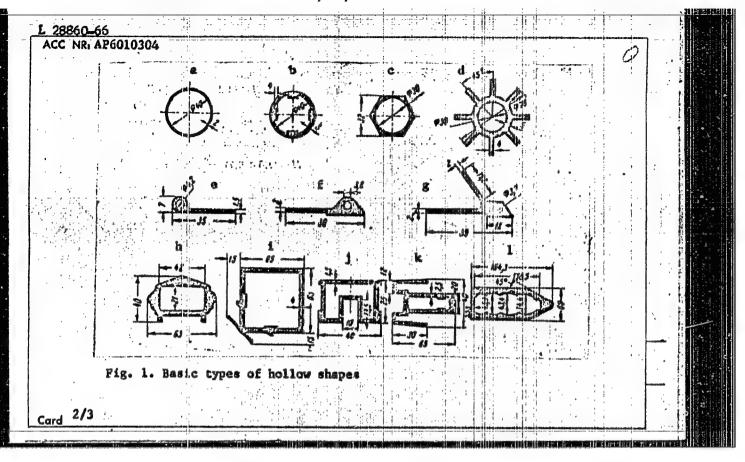
GUN, G.Ya.; POLUKHIN, P.I.; PRUDKOVSKIY, B.A.; POLUKHIN, V.P.; XERMANOK, M.Z.

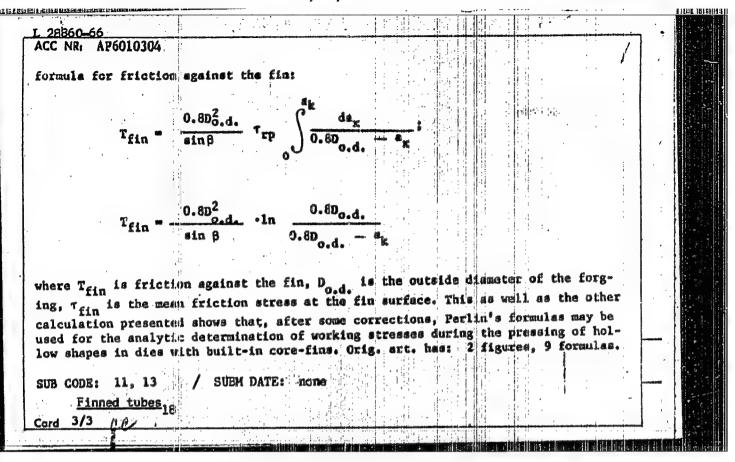
Calculating strain hardening and the temperature field during extrusion. Izv. vys. ucheb. zav.; tavet. met. 8 no.4:134-139 65. (MIRA 18:9)

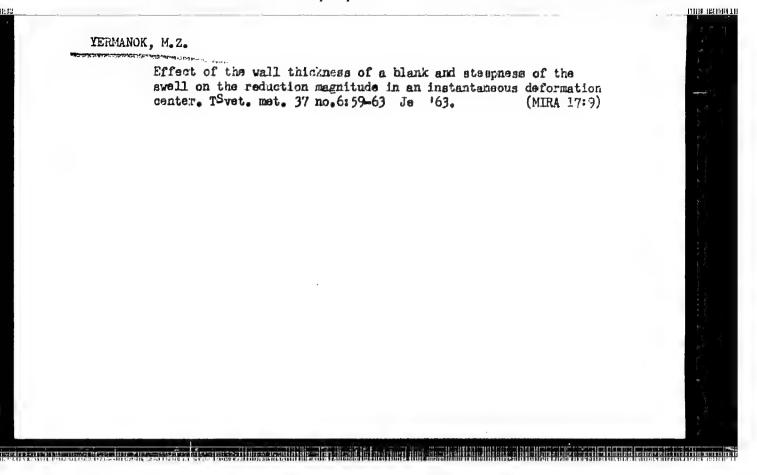
1. Kafedra tekhnologii i avtomatizatsii prokatnogo proizvodstva Moskovskogo instituta stali i splavov.

| UTHOR: Yermanok, M. Z.; Skoblov, L. S.; Filing, T. H. RG: none ITLE: Calculation of working stresses during pressing of hollow shapes in dies with built-in core-fin OURCE: Tsvetnyye metally, no. 3, 1966, 74-77 OPIC TAGS: stress analysis, die, metal pressing, metal friction, friction BSTRACT: The Al and Mg alloy shapes forged in core-fin dies may be divided into five easic groups (Fig. 1): a, with cylindrical external and internal contours, round cubes; b - with cylindrical external contour and shaped internal contours, round cubes; b - with cylindrical external contour and shaped internal contour; c, d - with shaped external contour and cylindrical internal contour; a, f, g, loop type (the area of orifice for these 3 groups of shapes is incommensurably small compared with the cross sectional area of the shape); h, i, j, k, l - with shaped external and internal contours. In this connection, the author corrects the known formulas of presence of the pressing of round tubes in core-fin dies (Perlin, I. L. Taoriya pressovaniya metallov. Izd-vo Metallurgiya, 1964), since Perlin failed to take into account the friction of metal against the die core-fin. Assuming that this fin represence of the state of the sta | 28860-66 ENP(k)/ENT(1) | , | OURCE CODE: UN | (101391891) | 10074/0077 | |
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| OURCE: Tsvetnyye metally, no. 3, 1966, 74-77 OPIC TAGS: stress analysis, die, metal pressing, metal friction, friction BSTRACT: The Al and Mg alloy shapes forged in core-fin dies may be divided into five asic groups (Fig. 1): a, with cylindrical external and internal contours, round ubes; b - with cylindrical external contour and shaped internal contour; c, d - ith shaped external contour and cylindrical internal contour; e, f, g, loop type the area of orifice for these 3 groups of shapes is incommensurably small compared ith the cross sectional area of the shape); h, i, j, k, l - with shaped external and internal contours. In this connection, the author corrects the known formulas of presing stress for the pressing of round tubes in core-fin dies (Perlin, I. L. Teoriys | kG: noue | * . | | | the E | |
| DRIC TAGS: stress analysis, die, metal pressing, metal friction, friction astract: The Al and Mg alloy shapes forged in core-fin dies may be divided into five asic groups (Fig. 1): a, with cylindrical external and internal contours, round ubes; b - with cylindrical external contour and shaped internal contour; c, d - ith shaped external contour and cylindrical internal contour; a, f, g, loop type the area of orifice for these 3 groups of shapes is incommensurably small compared ith the cross sectional area of the shape); h, i, j, k, l - with shaped external and internal contours. In this connection, the author corrects the known formulas of presing stress for the pressing of round tubes in core-fin dies (Perlin, I. L. Teoriya | ith built-in core-fila | | | ing of hollow sta | pes in dies | |
| the area of orifice for these 3 groups of shapes is incommensurably small compared the area of orifice for these 3 groups of shapes is incommensurably small compared ith the cross sectional area of the shape); h, i, j, k, l - with shaped external and ith the cross sectional area of the shape); h, i, j, k, l - with shaped external and ith the cross sectional area of the shape); h, i, j, k, l - with shaped external and ith the cross sectional area of the shape); h, i, j, k, l - with shaped external and ith the cross sectional area of the shape; h, i, j, k, l - with shaped external and ith the cross sectional area of the shape; h, i, j, k, l - with shaped external and ith the cross sectional area of the shape; h, i, j, k, l - with shaped external and ith the cross sectional area of the shape; h, i, j, k, l - with shaped external and ith the cross sectional area of the shape; h, i, j, k, l - with shaped external and ith the cross sectional area of the shape; h, i, j, k, l - with shaped external and ith the cross sectional area of the shape; h, i, j, k, l - with shaped external and ith the cross sectional area of the shape; h, i, j, k, l - with shaped external and ith the cross sectional area of the shape; h, i, j, k, l - with shaped external and ith the cross sectional area of the shape; h, i, j, k, l - with shaped external and ith the cross sectional area of the shape; h, i, j, k, l - with shaped external and ith the cross sectional area of the shapes; h, i, j, k, l - with shaped external and ith the cross section area of the shapes; h, i, j, k, l - with shaped external and ith the cross section area of the shapes; h, i, i, j, k, l - with shaped external and ith the cross section area of the shapes; h, i, i, j, k, l - with shaped external and ith the cross section area of the shapes; h, i, i, j, k, l - with shaped external and ith the cross section area of the shapes; h, i, i, j, k, l - with shaped external and ith the cross section area of the shapes; h, i, i, j, k, l - with shaped external and ith the cross sect | BSTRACT: The Al and Mg | alloy shapes in with cylindrical external | orged in core- | Ein dies may be d and internal cont and internal cont | ivided into five purs, round pur; c, d - | A) 110 |
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8/125/60/000/012/004/014 A161/A030

AUTHORS: Brodskiy, A.Ya; Fridman, A.M; Yermanck, Ye.Z; Frolov, S.A.

TITLE: Resistance Welding of 30Kh02S Reinforcement Steel for Pre-Stressed Reinforced Concrete Structures

PERIODICAL: Avtomaticheskaya svarka, 1960, No. 12, pp. 28 - 36

TEXT: The weldability of 30X Γ 2C (30KhG2S) reinforcement steel in resistance welding machines has been investigated and practical recommendations are given. The standard composition of this steel (GOST 5058-57) is: 0.26 - 0.35% C; 0.6 - 0.9% Si; 1.2 - 1.6% Mn; 0.6 - 0.9% Cr; not above 0.3% Ni and Cu (each): the mechanical properties: conditional yield limit $\sigma_{0.2} > 60 \text{ kg/mm}^2$; ultimate strength $\sigma_{0.2} > 90 \text{ kg/cm}^2$; elongation $\sigma_{0.2} > 60 \text{ kg/mm}^2$; ultimate around a mandrel with diameter equal to 3 diameters of the tested rod. Rods used for experiments were periodical, with 1^{14} - 28 mm diameter, produced by the Stalino and Magnitogorsk metallurgical works. Round test specimens with sharp notch in different heat affected zones, so-called UHNNC(Tanips specimens) were used with success first or all with other reinforcement steel, but had to be replaced with Menazhe (Russian transliteration) notch specimens for 30KhG2S because of its very high notch sensitivity. It proved also very sensitive to inaccuracy of connection Card 1/4

S/125/60/000/012/004/014 A161/A030

Resistance Welding of 30KhG2S Reinforcement Steel for Pre-Stressed Reinforced Concrete Structures

angle in cross connections as well as to burns in machine grips during resistance welding. It is recommended to prevent burns by using electrodes with a wide contact surface, to raise the gripping effort, to carefully clean the surface of electrodes and rods, and to reduce the current density in these spots, which is possible by not only conducting current to the bottom electrodes but also to the upper hold-downs made from copper alloy. In view of the high sensitivity to heating time with butt welding, preheating should be carried out, (not too drastically) - e.g. continuous fusing is not premissible - for chilling in the heat-affeeted zone reduces strength through the formation of martensite spots (Fig. 3) which affects deformability and thus causes cracks. The formation of martensite can be prevented by heat treatment between the electrodes of resistance welding machines fitted with special automatic devices. [Abstracter's note: No details of such devices are mentioned]. The optimum welding process conditions were found in experiments in an ACM\$\phi\$-75 (ASIF-75) welder with a recorder which enabled the duration and temperature of preheating, the magnitude of upsetting, the number of preheating cycles, and the total welding time to be determined. The optimum values of the following major parameters were determined: setting length 1 yCT Card 2/4

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Resistance Welding of 30KhG2S Reinforcement Steel for Pre-Stressed Reinforced Concrete Structures

fusion length $l_{OD,\Lambda}$, and upsetting length l_{OC} , as well as the transformer stage. The optimum process was determined by the shape of the curves of breaking load, bending angle and impact strength in butt joints. For medium-diameter reinforcement rods the lycr , long and loc values must be 2.8; 0.7 and 0.35 respec-Joints in 20 and 28 mm diameter rods were tively. Butt d so welded in ASIF-75 and Mcp-100 (MSR-100) welders. In spot welding of cross joints the weldability of 30KhG2S steel was much lower than of Cr.5 (St.5), and the highest possible mechanical strength was obtained with about 2 sec. holding (St.5 requires three times as much holding). With St.5 rods, spot welded connections can be obtained with mechanical strength not below the strength of the base metal, regardless of the transformer stage, but in 30KhG2S spot welds the strength can drop drastically and be very uneven. The cause is the presence of martensite and heterogeneous structure. The properties of cross joints can appearantly be improved by heat treatment in the welding machine (between electrodes) (Ref. 3) (A. Ya. Brodskiy, P.I. Sokolovskiy. A.M. Fridman, "Avtomaticheskaya svarka", No. 3, 1958). Conclusions: 1) Resistance welding with 30KhG2S reinforcement steel is more difficult than with other Soviet reinforcement steel grades, but butt joints Card 3/4

3/125/60/000/012/004/014 A161/A030

Resistance Welding of 30Kh02S Reinforcement Steel for Pre-Stressed Reinfor ed Concrete Structures

are possible with ultimate strength not below the standard minimum for this steel. 2) Smooth (r.3 (St.3) steel rods can be joined with 30KhG2S rods by spot welding into cross joints without weakening the rods. Cross joints of 30KhG2S with 30KhG2S have not more than 86% of initial metal strength before welding. 3) Brittleness is the drawback of all joints in 30KhG2S steel rods made by resistance welding, but it may be eliminated by heat treatment between electrodes. There are 6 figures and 3 Soviet references.

ASSOCIATIONS: Tanil stroitel nykh konstruktsiy ASiA SSSR (Tanil of Construction Frameworks AS and A USSR). A.Ya. Brodskiv and A.M. Fridman; NII zhelezobeton pri Mosgorispolkome (Scientific Research institute for Reinforced Concrete at Moscow City Executive Committee), Ye.Z. Yermanok: MVTU imeni Baumana (MVTU imeni Bauman), S A Frolow

SUBMITTED:

March 3, 1960

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| AUTHORS: Yerman | OK 18 60; | KOOIII, I. | Z, t Shuvarikov | . V. M.; Gramby | sk17, B. T. | |
| ORG: none | | | 4.44.55 | | 44 | |
| TITLE: A method | for contact | arc weldin | g of T-joints. | Class 21, No. 1 | 76336 | |
| SOURCE: Byullet | en' izobrete | miy i tovar | nykh znakov, no | . 22, 1965, 40 | | |
| TOPIC TAGS: welding | ling, weldin | g electrode | , welding equip | ment, wilding te | chnology, are | |
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| ABSTRACT: This between rods and the welded joint of an electrode | plates. To the headin provided wit | facilitate g is produc h a groove. | the process and ed in the course | d to improve the | quality of | |

Card 1/1 Pub. 121 - 20/28

Authors : Pogodin A. S., Eng.; Bulatov, N. I. Tormanov, B. V., Ing.; and Eurkov, V. I., Eng.

Title t Problems dealing with a non-mimsograph method of suproducing drawings

Periodical : Vest. mesh. 35/6, 75 - 80, Jun 1995

Abstract : A series of latters submitted to the editor of this publication by implication

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SOV/32-25-4-24/71

AUTHORS:

Yermanovich, N. A., Longinov, M. F., Orlov, L. G., Utevskiy, L.M.

TITLE:

Examination of Interdendritic Nonmetallic Streaks in Cast Steel (Obnaruzheniye mezhdendritnykh nemetallicheskikh prosloyek v

littoy stali)

PERIODICAL:

Zavodskaya Laboratoriya, 1959, Vol 25, Nr 4, pp 440-442 (USSR)

ABSTRACT:

Sites of fracture in some structural steels (40 KhNMA, 12Kh2N4A, 30KhVFYu, 30 KhGSA, 30 KhGSNA) pointed to a destruction of the metal along the boundary of the primary grain. On the strength of tests it is assumed that nitrides, especially aluminum nitride (I), accumulate at these boundaries and produce a weakening. This assumption was examined in the present case by means of an electron microscope and an electronograph. By an electrolytic heating, a thin coating layer was obtained at the site of fracture, which could be removed by the reagent according to Popova and examined. On the microphotograph of a fracture in the steel 40 KhNMA (Fig 1) one can well observe the inclusions, the forms of which are represented even better by the electron microscope (Fig 2). The phase composition of these inclusions was investigated by the X-ray structure- and electronographic method. In the X-ray picture (I) was observed in the

Card 1/2

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SOV/32-25-4-24/71

Examination of Interdendritic Nonmetallic Streaks in Cast Steel

steel 38 KhVFYu (I), and (I) and VN in samples with big faults, (I) and F₃Al₂(SiO₄)₃ in the steel 12 Kh2N4A - (I), and (I) in the steel 40 KhNMA - (I). The electronograms (Fig 3 for 40KhNMA) corresponded to a crystal lattice of (I). In order to convert structural components from a disperse to a crystalline form, the samples were treated in the vacuum (at 800° for 2 hours); a fine formation of stains (Fig 4) was observed and the distinct electronogram of a polycrystal (Fig 5) was obtained with three phases - a spinel lattice, (I) and a phase which could not be identified. A test storing in the vacuum at room temperature for some days showed a crystallization, the electronogram of which is described (Table). There are 5 figures and 1 table.

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ASSOCIATION:

Zlatoustovskiy metallurgicheskiy zavod, Tsentral'nyy nauchnoissledovatel'skiy institut chernoy metallurgii (Zlatoust Metallurgical Works, Central Scientific Research Institute of Iron Metallurgy)

Card 2/2

18 (7) AUTHORS:

Longinov, M. F., Yermanovich, N. A. SOV/32-25-5-17/56

TITLE:

Separation and Analysis of Steel Impurities (Resdeleniye i

analis vklyucheniy v stali)

PERIODICAL:

Zavodskaya Laboratoriya, 1959, Vol 25, Nr 5, pp 571-573 (USSR)

ABSTRACT:

A method is described, which allows a separation of the steel impurities (I) from the carbides (II) without a chemical treatment of the anode precipitate as well as a separation of (I) in individual phases for the X-ray structural and electronographic analysis. For this purpose the authors comminuted the anode precipitate soaked in alcohol with an electromagnetic vibrator (Fig 1) for 2-3 hours. The (II) whose dispersity is considerably higher remain dispersed and thus oun be separated from the deposited (I). The ferromagnetic phase is then separated from (I) with a magnet and the other phases are separated according to the specific weight. The latter may take place mechanically with a special apparatus (Fig 2) on which the interaction between centrifugal force and gravity is made use of. To be true, this method does not allow the separation of (I) having a dispersion degree equal to that of (II). This, however, can be attained by a continuous

Card 1/2

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Separation and Analysis of Steel Impurities

SOY/32-25-5-17/56

decarbonization of steel up to a low carbon content, in which case the total carbon passes over into the solid solution during hardening of the sample and no (II) is formed. This decarbonization of the sample takes place in a closed tube (Fig 3) which is kept at 1150-1250° during 80-100 hours. In this way sulphides (CuS, MnS), oxides (MgO, Al₂O₃) nitrides (AlN, VN) could be determined in the steel 40 KhNMA. It was proven that at the grain boundaries in the steel 30 KhVFYu mitrides (AlN, VN) having a pink and blue coloring may be found. In steel 12 KhMF large amounts of copper sulphide steel impurities (Fig 4) were found and the angular c ystals observed in steel Kh 17 N 2 were identified as MgAl₂O₃ crystals. There are 4 figures.

ASSOCIATION:

Zlatoustovskiy metallurgicheskiy savod (Zlatoust Metallurgical Plant)

Card 2/2

S/130/63/000/003/001/001 A006/A101

AUTHORS:

Khasin, C. A., Yermanovich, N. A., Pribytkova, K. N.

TITLE:

Improving the ductile properties of high-chromium steels

PERIODICAL: Metallurg, no. 3, 1963, 27 - 29

TEXT: The authors studied the effect of hot deformation temperature, cooling methods after rolling, and variants of heat treatment upon the ductile properties of high-chromium steels. Square and round specimens were subjected to the following variants of forging, heat treatment and cooling: preheating for forging from 1,000 - 1,200°C; forging completed at 700 - 940°C; heat treatment at 780 and 900°C during 4 hours; quenching in water and air. It was found that the ductility of steel, determined from the magnitude of contraction after forging, increased with lower forging temperatures. A considerable increase in ductility occurs when the temperature of completed forging is below 800°C. There was no marked difference between the properties of metals, cooled after forging in air, water and cinder. Heat treatment of forged metal at 780°C for 4 hours and cooling in water raises considerably the ductility of the steel and is re-

Card 1/2

8/130/63/000/003/001/001

Improving tin ductile properties of high-chromium steels ACC6/A1C1

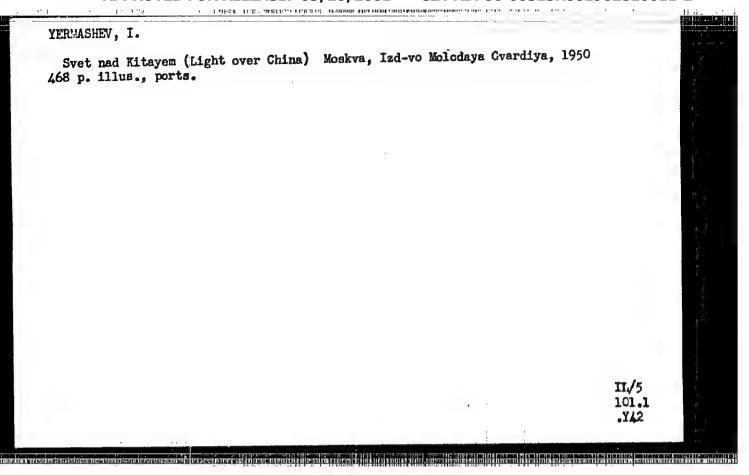
commended for steels which do not possess the required ductile properties after forging and rolling. Changes in the microstructure, depending upon heat treatment conditions, were studied by heating square steel specimens to temperatures ranging from 700 - 1,100°C with different holding time, and dooling with the furnace, in air or in water. After heat treatment at over 800°C, the ductile properties of the steel remain low; they are normal at 780°C heating for 4 - 5 hours. There are 3 figures and 2 tables.

ASSOCIATION: Zlatoustovskiy metallurgicheskiy zavod (Zlatoust Metallurgical Plant)

Card 2/2

PERLIN, I.L., OLEBOV, Yu.P., YERMANYUK, M.Z.

Character of the dependence of the resistance to deformation on the degree of deformation in recrystallization processes following the pressure working of metals. Inv. vys. ucheb. sav.; tsvet. met. 7 no. 4:135-141 764 (MIRA 19:1)



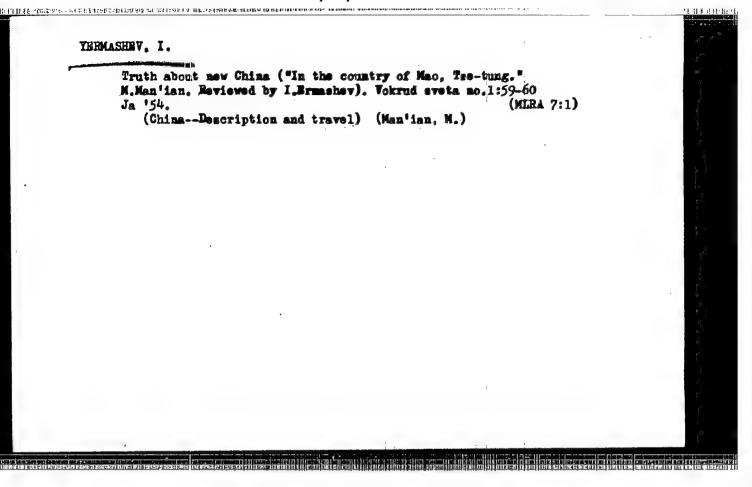
YERRASHEV, I.

Tibet

New book about Tibet ("Tibet". B. V. Yusov. Reviewed by I Yermashav.) Vokrug sveta, no. 8 1952.

2

9. Monthly List of Russian Accessions, Library of Congress, November 1953, Uncl



MARKOV, N.M., kand.tekhn.nauk; TERENT: YEV, I.K., kand.tekhn.nauk; YEDMASHOV, N.M., insh.

Some results of the experimental study of the effect of steam moisture on the characteristics of turbine stages. Izv. vys. ucheb. zav.; energ. 6 no.3:68-74 Mr 163. (MLRA 16:5)

1. TSentral nyy kotloturbinnyy institut imeni I.I.Polsunova. Predstavlena sektsiyey parovykh i gazovykh turbin. (Steam turbines)

APPROVED FOR RELEASE: 03/20/2001 CIA-RDP86-00513R001962810011-2"

(MIRĂ 18:9)

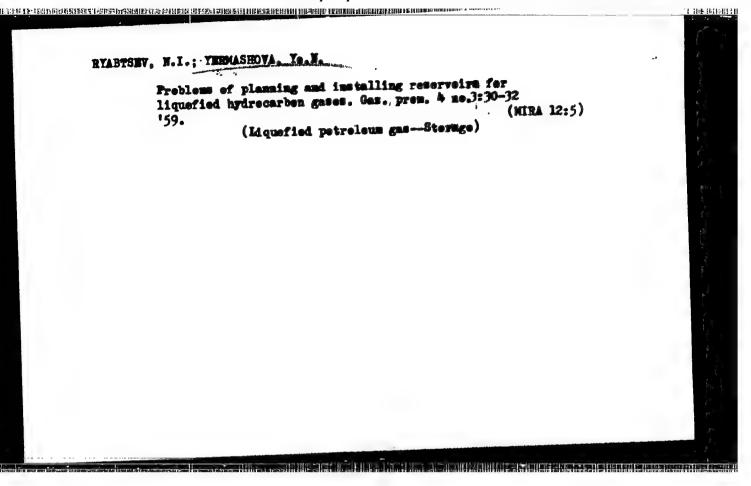
YERMASHOV, N.N., inzh.; MARKOV, N.M., doktor tekhn. nauk, prof. Development of instruments for determining the degree of steam moisture. Izv. vys. ucheb. zav.; energ. 8 no.8:96-100 Ag '65.

1. TSentral'nyy kotloturbinnyy institut imeni I.I. Polzunova.

NYADTSEV. N., kand.tekhn.nauk; YERMASHOVA, Ye., insh.

Using liquefied hydrocarbon gases for compensating daily and seasonal fluctuations and substituting other gases. Zhil.-kow. khos. 8 no.1:12-15 '56. (NIRA 11:1)

(Gas distribution)



66473

21(8) 5.4500(B)

SOV/20-129-1-19/64

AUTHORS:

Starodubtsev, S. V., Academician, Academy of Sciences,

UzbekskayaSSR, Ablyayev, Sh. A., Yermatov, S. Ye.

TTTLE:

Variation of Adsorptive Properties of Silicagel Under the

Action of Gamma-irradiation

PERIODICAL:

Doklady Akademii nauk SSSR, 1959, Vol 129, Nr 1,

pp 72 - 73 (USSR)

ABSTRACT:

Ionisation and excitation of atoms and molecules as well as displacement of the atoms is caused in solids under the action of penetrating rays. It becomes manifest by an external variation of the mechanical, optical, electrical, physico-chemical, and chemical properties of the bodies. Different preliminary works dealing with this subject are shortly reported. The properties of irradiated silicagel have hitherto been investigated only by A. N. Terenin et al (Refs 6,7). These authors irradiated silicagel by ultraviolet

rays and showed, that a process occurs, similar to that on heat treatment, i. e. hydroxyl groups are separated and free valences occur at the surface. Present paper describes

the experimental investigation of adsorptive properties, Card 1/3

Variation of Adsorptive Properties of Silicagel SOV/20-129-1-19/64 Under the Action of Gamma-irradiation

basing on the adsorption of gases, measured by means of thermocouples and ionization manometers. Experimentally produced silicagels of the type KSK were used for this experiment. Prior to the investigation, these silicagels were subject to careful, long lasting heat treatment, and were then irradiated by Y-rays (dose rate 15.104 to 35.104 r/hour, total dosage 1.5.106 to 2.106 r) in evacuated glas tubes (which were provided with manometer tubes). The following is shown by the results of these investigations: The adsorptive power of silicagel increases remarkably under the influence of Y-rays, and the amount of the gas, adsorbed by the irradiated silicagel increases up to a known boundary value, with increasing irradiation dose. The first diagram shows the change of the adsorptive properties of silicagel with respect to H2, N2 and Ar at low pressures, and the second diagram shows the same for CO2, CO, NH3, C2H4 and H2S, under the condition, that pressures of 1 - 10-1 torr prevailed before the irradiation. According to these diagrams, the adsorptive power of the irradiated silicagel samples increases differently for different gases.

Card 2/3

66473

Variation of Adsorptive Properties of Silicagel Under the Action of Gamma-irradiation

SOV/20-129-1-19/64

At comparatively high gas pressures (4 torr) the irradiated silicagel can adsorb an amount of hydrogen of 2.5.10-5 of its total weight. In this experiment, it is important and interesting, that silicagel assumes its previous properties, if heated to 100°. At room temperature, almost no such "annealing" of the irradiation effect may be noticed. Obviously, the changes of the adsorptive properties of silicagel under irradiation with y-rays may be explained by the separation of hydroxyl groups and the formation of free valences at the surface as well as by the interruption of the bonds between the free radicals (which were formed during the primary heat treatment) and by the high ionization of the gas (the adsorbate), effecting an increase of the adsorptive power of silicagel. There are 3 figures and 7 references, 6 of which are Soviet.

SUBMITTED:

June 9, 1959

4

Card 3/3

33100 \$/638/61/001/000/025/056 B104/B138

5.4600

AUTHORS: Ablyayev, Sh. A., Yermatov, S. Ye., Starodubtsev, S. V.

TITLE: Variation in adsorption properties of silica gel during

gamma irradiation

SOURCE: Tashkentekaya konferentsiya po mirnomy ispol zovaniyu atomnoy

energii. Tashkent, 1959. Trudy, v. 1. Tashkent, 1961,

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174 - 177

TEXT: The adsorption properties of industrial KCK (KSK) silica gel were determined from the amount of gas absorbed, and by measurements with thermocouple and ionization manometers. Before the experiments, the samples were carefully heat-treated, sealed in evacuated ampoules, and exposed to gamma rays. Radiation dose was 150 - 350,000 r/hr reaching a total of up to 2 million r. The adsorption properties of silica gel increase considerably during irradiation, and differ for different gases. Some gases, such as argon or hydrogen sulfide, are hardly adsorbed at all. Amounts of gas additionally adsorbed during irradiation:

Card 1/3

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Variation in adsorption ...

Gas

Additionally adsorbed gas amount, moles/g

12 Hydrogen 8 Mitrogen 18 Carbon dioxide Ammonia gas 0.5 Ethylene

When the silica gel is heated to 100°C, its properties return to their initial state, i.e. annealing occurs. The increase in adsorption power remains practically constant at room temperature. The lower the temperature (down to -150°C), the more rapid the adsorption process. The adsorption power of silica gel increases with decreasing temperature, but the increase is greater during gamma irradiation. Results are explained as follows: (1) The hydroxyl group is destroyed by irradiation, and free valences are formed; (2) electrically charged active centers are formed; (3) the bonds between free radicals are ruptured. A. N. Terenin et al. (DAN SSSR, 66, 885, 1949) are mentioned. There are 3 figures, 1 table, and 6 references: 5 Soviet and 1 non-Soviet.

Card 2/3

S/638/61/001/000/025/056 B104/B138

Variation in adsorption ...

ASSOCIATION: Fiziko-tekhnicheskiy institut AN UzSSR (Physicotechnical Institute AS Uzbekskaya SSR)

X

Card 3/3

S/166/50/000/006/008/008 C111/C222

AUTHORS: Ablyayev, Sh.A., Yermatov, S.Ye. and Starodubtsev, S.V., Academician of the Academy of Sciences Uzbekskaya SSR.

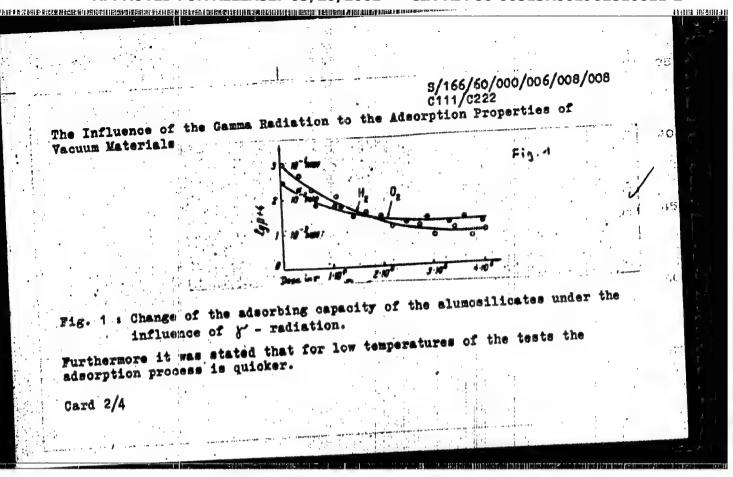
TITLE: The Influence of the Gamma Radiation to the Adsorption Properties of Vacuum Materials

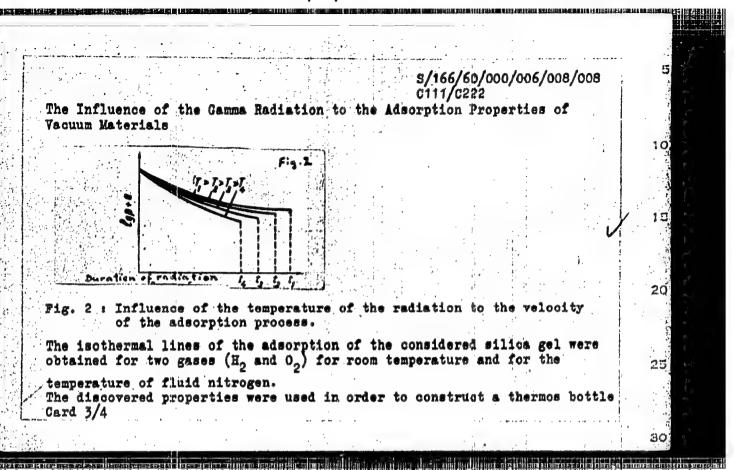
PERIODICAL: Izvestiya Akademii nauk Uzbekskoy SSR, Seriya fizikomatematicheskikh nauk, 1960, No. 6, pp. 95 - 95

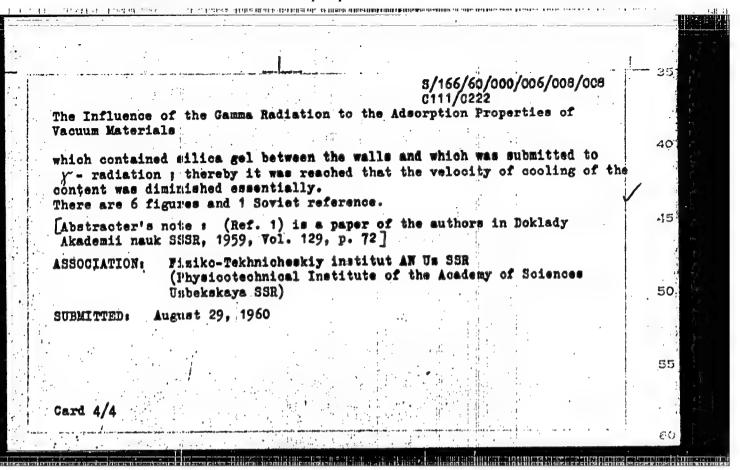
TEXT: In (Ref. 1) the authors showed that the adsorption properties of silica gel are changed essentially by Y - rays Co⁶⁰. The present paper is a continuation of (Ref. 1). The authors investigate the adsorption properties of the types K(K(KSK) and ACM(ASM) of the silica gel properties of the types K(K(KSK) and ACM(ASM) of the silica gel and of the alumosilicates. It was stated that the adsorbing capacity of the alumosilicates after a Y - radiation increases somewhat and the adsorbing capacity of the silica gel increases strongly.

Card 1/ 4

30







YERMATOV, S., CAND PHYS-MATH SCI, "CHANGES IN THE ADSORP-TION PROPERTIES OF SILICA GEL UNDER RECENTED GAMMA-RAYS."

TASHKENT, 1961. (ACAD SCI UZSSR. PHYS-TECH INSTITUTE).

(KL-DV, 11-61, 208).

-10-

8/844/62/000/000/119/129 D207/D307

AUTHORS: Starodubtsev, S. V., Ablyayev, Sh. A., Vasil'yeva, Ye. K.

and Yermatov, S. Ye.

TITLE: Effect of p radiation on adsorption properties of silica

gels

SOURCE: Trudy II Vsesoyuznogo soveshchaniy po radiatsionnoy khi-

mii. Ed. by L. S. Polak. Moscow, Izd-vo AN SSSR, 1962,

689-692

TEXT: Factory-made silica gel of KCK (KSK) grade was heat-treated in evacuated ampoules and then subjected to 7 rays at dose rates up to 340,000 r/hour. Adsorption was then investigated by admitting a gas or vapor to the ampoules held at temperatures from +20°C to liquid-nitrogen temperature. On cooling, the adsorption ability of silica gel increased even without irradiation, but 7 rays intensified this increase. The amount of oxygen adsorbed rose linearly with pressure of the admitted gas or vapor in unirradiated and irradiated silica gel, indicating the same nature of adsorption cen-

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Effects of) radiation ...

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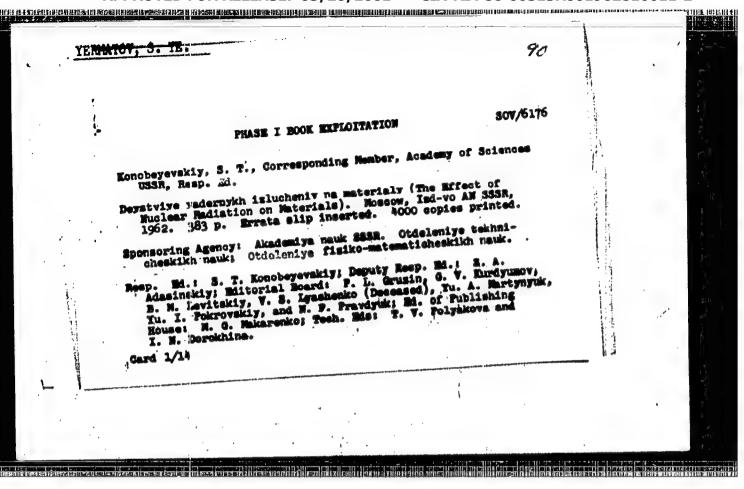
ters in both cases. The silica gel surface became saturated with adsorption centers at doses of 2 - 3 x 10⁶ r. Gamma irradiation raised the amount of heptane vapor that could be adsorbed on silica gel (this effect was smaller than for the majority of gases) but made no difference to the adsorption of benzene vapor. Irradiation of aqueous solutions of ammines of the [Co(NH₃)₆]Cl₃ type in direct contact with silica gel raised the amount of liquid adsorbed because of ra-

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with silica gel raised the amount of liquid adsorbed because of radiation-induced chemical reactions in the solutions rather than due to changes on the silica gel surface. Gamma-irradiation raised also the amounts of oxygen and hydrogen that could be adsorbed by aluminosilica gel. A practical application of these observations consisted of placing practivated silica gel between the walls of a thermos flask. This improved the vacuum between these walls, by adsorbing more gas than unirradiated silica gel, and thus reduced heat transmision through the walls. Such thermos flasks were prepared at the Ashkhabadskiy stekol nyy kombinat im. V. I. Lenina (Ashkhabad Glass Combine im. V. I. Lenin). There are 7 figures.

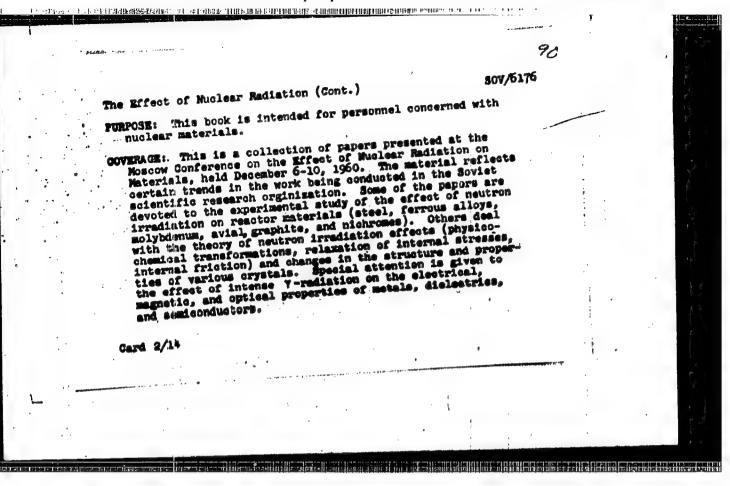
ASSOCIATION: Fiziko-tekhnicheskiy institut AN UzbSSR (Physico-Technical Institute AS UzSSR)

Card 2/2



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ACCESSION NR: AT3007248

- S/2952/63/000/000/0011/0018

AUTHORS: Starodubtsev, E.S. V.; Ablyayev, Sh.A.; Yermatov, S.Ye; Pulatov, U.U.

TITLE: Changes in adsorptivities of silicagels and zeolites under the action of high-frequency discharges

SOURCE: Radiatsion. effekty* v tverd. telakh. Tashkent, Izd-vo AN UzbSSR, 1963, 11-18

TOPIC TAGS: adsorption, adsorptivity, silicagel, zeolite, electric discharge, slow electron, gamma ray, cosmic radiation, temperature effect, isotherm, high-frequency discharge

ABSTRACT: The paper reports the basic results of an experimental investigation of the effect of fluxes of slow electrons on the adsorption properties of synthetic zeolites and silicagels. Test objects were: Silicagel Mark KSK and synthetic zeolites of the types 4A (NaA) Gor'kovskoye, CaA 5A Gor'kovskoye, 13x(Nax) Gor'kovskoye, 4A (NaA) Groznoye, and CaA 5A Groznoye. High-frequency electric discharges served as slow-electron sources. The changes in the adsorptional properties were investigated experimentally by the adsorption of gases by adsorbents measured by manometric tubes. The specimen adsorbent, contained in a glass ampoule (A), is

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ACCESSION NR: AT3007248

first heated to 350-400°C under continuous evacuation. The A is then filled with . the test gas from a reservoir V, following the evacuation of the air from the entire system down to 10⁻³ to 10⁻⁴ mm Hg. The gas is permitted to enter the adsorbent container A up to a specified pressure, whereupon A is soldered tight and thus cut off from the vacuum equipment and held at room temperature until the establishment of an equilibrium pressure, which is of the order of 10" mm Hg. The instrument is then exposed to the action of the high-frequency discharges. Zeolites: Test results, plotted in the form of curves, show that all types of zeolites gain in adsorptional capacity under the effect of slow electrons. These changes increase with increasing irradiation time up to a specified limit and then achieve saturation. after about 6 to 10 min. Optimal results were obtained with the Gor'kovskoye zeolites of the types 13x(Nax) and CaA 5A. Isotherms of ordinary and induced adsorption of zeolites with reference to dry air at temperatures of 20 and -196°C were derived. Silicagels: Exposure to the discharges increased the adsorptivity of silicagel substantially. Saturation at any given oscillatory power was achieved after 8-15 minutes. Isotherms of ordinary and induced adsorption of silicagel with respect to dry air in the 10-1 to 10-3-mm-Hg range were obtained at temperatures of 0, +30, +60, and -196°C. Adsorbent temperature exerted a noticeable effect on the magnitude of both ordinary and induced adsorption. The adsorptivity of silicagel and zeolites increases with decreasing temperatures even without irradiation.

Card 2/3

THE MEST AND THE PROPERTY OF THE PROPERTY OF THE WINDS AND AND ADDRESS OF THE PROPERTY OF THE ACCESSION NR: AT3007248 However, the changes are substantially greater under irradiation, and the adsorption is much more parmanent. The effect of lower temperatures is stronger on zeolites than on silicagels. Some light is shed on the effect of slow electrons and gamma-ray radiational effects on the surface layer and into the depth of an adsorbent. Orig. art. has: 7 figures. ASSOCIATION: none ENCL: 00 DATE ACQ: 140ct63 00 % SUBMITTED: OTHER: 000 NO REF SOV: PH-EE, MA SUB CODE: Card

\$/2952/63/000/000/0019/0021

ACCESSION NR: AT3007249

AUTHORS: Starodubtsev, S. V.; Ablyayev, Sh. A.; Yermatoy, S. Ye; Azizov, S. A.

TITLE: Effect of gamma radiation on the adsorptional properties of synthetic zeolites,

SOURCE: Radiatsion. effekty* v tverd. telakh. Tashkent, Izd-vo AN UabSSR, 1963, Saa

19-21

TOPIC TAGS: adsorption, ordinary adsorption, supplementary adsorption, radiation-induced adsorption, zeolite, gamma ray, gamma-ray-induced adsorption, radiation; gamma radiation, temperature effect, isotherm

ABSTRACT: The paper describes an experimental investigation of the effect of gamma rays on the adsorptivity of synthetic zeolites. The tests were performed by the ordinary volumetric method on 3 Gor'kovskoye specimens of the types 4A (NaA), CaA 5A, and 13x (Nax), and two Groznoye specimens 4A (NaA) and CaA 5A. The zeolite specimens were first heat-treated thoroughly at temperatures of 350-400°C at pressures between 10⁻¹ and 10⁻⁶ mm Hg for several hours. The zeolites were then exposed to gamma rays of a radiation dosage rate of 150 to 350,000 r/hr, with a total dose of 2 to 3.100 r. The adsorptivity of the zeolites was found to be

Cord 1/3

ACCESSION NR: AT3007249

significantly increased; the increase grew to a certain limit depending on the intensity of the radiation dose. The effect of the glass on the test results was determined by identical control ampoules with O and H, with and without adsorbents, exposed to gamma radiation. It was found that the ampoules not containing adsorbents maintained a constant gas pressure. Therefore, the effect of the glass was found to be nil. It was found that the adsorption temperature affects the magnitude of the gamma-ray effect substantially. The radiational effect decreases at elevated temperatures, that is, a radiational anneal occurs. The effect disappears completely at 300-400°C. It is noted that following an anneal the limiting pressure occurs at lower values of the radiational dose. Comparative isotherms of supplementary and ordinary adsorption of an irradiated zeolite were plotted for dry air at -1960 and at room temperature. The nature of the radiation effect observed is explained by the knocking out of a Compton electron by a primary gamma quantum, whereupon the fast electrons pass along a path of 2-3 mm within the zeolite. Having expended their energy on the ionization of the matter, they form a large number of relatively slow electrons with energies of the order of tens of ev. The resulting strong ionization forms negative and positive ions which produce excitaitions and other defects of various kind. The number of possible defects per gamma quantum ordinarily amounts to several tens of thousands; these defects do not differ from those obtainable by UV and X-ray impingement. The supplementary

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adsorption of gases on the zeolites occurs in such defects. Orig. art. has: 3 figs.

ASSOCIATION: none

SUBMITTED: 00 DATE ACQ: 14Oct63 ENCL: 00

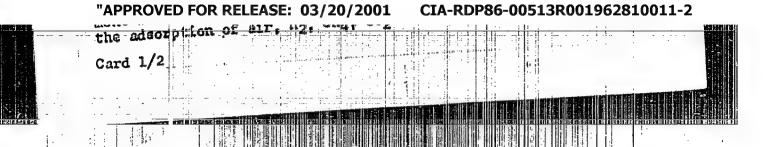
SUB CODE: MA, PA, EE, CH NO REF SOV: 005 OTHER: 000

S/109/63/006/002/019/028
D413/D308

Starodubtsev, S.V., Ablyayev, St.A., Yermatov, S.Ke.
and Pulatov, U.

The effect of radio-frequency discharges on the adsorption properties of silica g.l.
sorption properties of silica g.l.
Radiotekhnika i electronika, v. 8, ro. 2, 1963,
328-330

Text:
Tex



The effect of radio-frequency ...

8/109/55/008/002/019/028 D413/D503

times was measured by manameter tubes. The resulting curves show increases it adsorption closely similar to those obtained by the action of Y-radiation, ranging from zero for He to a saturation value of 0.4 \$\mu\$ mole g-1 for H2. The induced adsorption disappears completely in baking at 350°C. Isotherns are also given for the induced adsorption of dry air at 0° 30° and 60°C over the range

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STARODUBTSEV, S.V., akademik; ABLYAYEV, Sh.A.; YERMATOV, S.Ye.; PULATOV, U.U.

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Charge in the adsorbing capacity of silica gel induced by high-frequency discharges. Izv. AN Uz. SSR. Ser. fiz.-mat. nauk no.6:77-78 '61. (MIRA 16:12)

1. Fiziko-tekhnicheskiy institut AN UzSSR. 2. Akademiya nauk UzSSR (for Starodubtsev).

فيسور وأرثامها ID/OU/GE LJP(a) L 2142-66 ENT(m)/EPF(c)/EPF(n)-2/ENP(t)/EMP(b) UR/0000/62/000/000/0366/0369 ACCESSION NR: ANSO23820 B Staredubtsev, S. V.; Ablyayev, Sh. A.; Yersetov, S. Ye. TITLE: Effect of gamma fluxes on the adsorptive properties of vacuum materials SOURCE: Sovembehaniye po probleme Devetvive vadernyth inlantenty na materialy.

Moscow, 1960. Devetvive yadernyth isluchenty na materialy (The offect of nuclear radiation on materials); doklady soveshchaniya. Hoscow, Ind-vo AN SSSR, 1962, TOPIC TAGS: eilica gel, aluminum silicatu, gamma irradiation, irradiation effect, ABSTRACT: The article continues the study of K-ray-induced changes in the adsorptive properties of KSK and ASH silica geldend plant-produced aluminosilicates. Oxygen and hydrogen were used as the adsorbed gases, and the radiation dose rate was (150-350) 103 r/hr. All the results showed an increase in adsorptive capacity that was much more pronounced in silica gels than in aluminosilicates. The temperature dependence of this redistion effect was investigated between +100 and -1300, and the adsorptive capacity was found to increase with decreasing temperature (this increase was much greater than that of nonigradiated samples). The adsorption isotherms were found to be linear both at room temperature and at the

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| liquid nitrogen temperature showed that equilibrium pre i.e., the adsorption is not approximation the additions obey the same laws as ordin gels to thus increase their | essure is establia : instantaneous. il active adsorpti ary centers on si : adsorptive capac | thed after a co The data indic ion centers pro lica gel. The ity was utilis | erthin time intract to a polyced by the Y a property of a sed for the cre | erval, first rays ilica stion |
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AUTHOR: Umarov, G. Ya.; Lyutovich, A. S.; Yermatov, S. Ye.; Karimov, F. R.

ORG: Physico-technical Institute, AN UzSSR, Tashkent (Fiziko-tekhnicheskiy institut AN UzSSR)

TITLE: The possibility of obtaining semiconductor and difficultly fusible materials with the aid of a jet discharge

SOURCE: AN SSSR. Sibirskoye otdeleniye. Izvestiya. Seriya tekhnicheskikh mauk, no. 3, 1966, 104-105

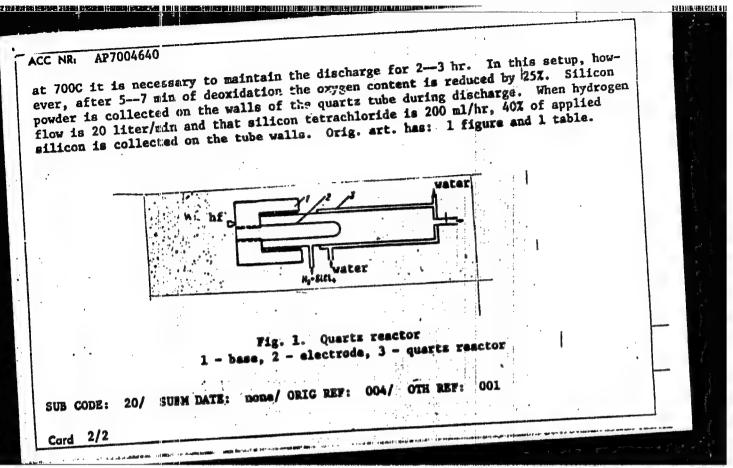
TOPIC TAGS: thermal reactor, oxidation reduction reaction, gas discharge, high frequency discharge, metal spide, weln could nuclear reactor.

ABSTRACT: A gas discharge setup (see Fig. 1) is described for deoxidizing such materials as silicon oxide and metallic oxides. The discharge in this water-cooled quartz reactor is maintained by 10-kw, 25-Mc, rf energy source and the raw materials are SiCl₄ and M₀O₃. The reactor is 75 cm long and 20 cm in diameter. When molybden-

um oxide is being reduced cooling is not necessary. The discharge is started at silicon electrode progressing to the surrounding mixture of hydrogen and silicon tetrachloride. When molybdenum oxide is being reduced the electrode is made of molybdenum. Under normal conditions to reduce molybdenum trioxide to dioxide state

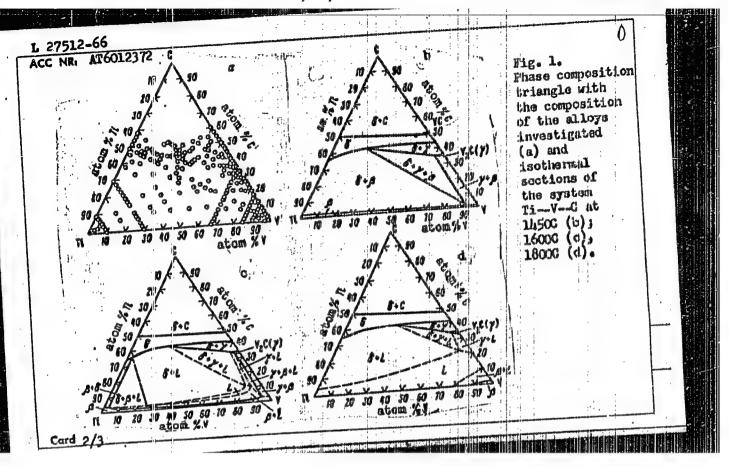
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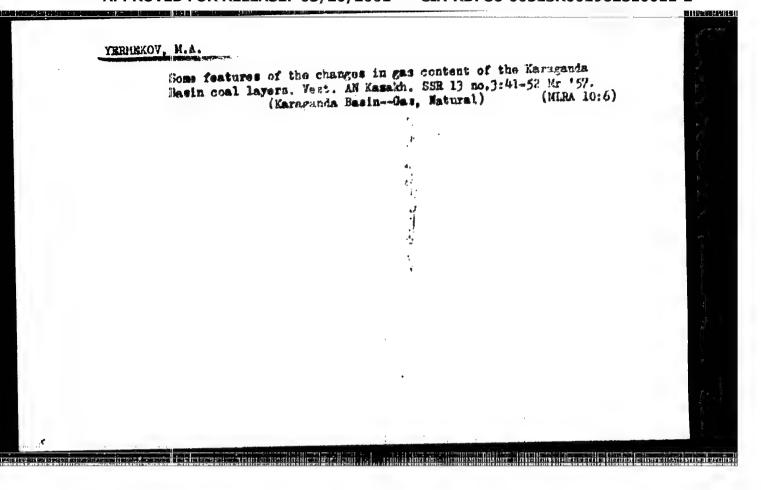
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L.L., insh.; GOLOMAZOV, V.A., insh.; BOBYLEVA, S.F.; LYSKOV,
L.L., prinimali uchastiyes BRIZHHEV, I.S.; SHCHETKIN, L.I.;
I.K.; Prinimali uchastiyes BRIZHHEV, I.S.; SHCHETKIN, L.I.;
YERMAJSKAYA, A.M.; ANDRIABOVA, A.L.; SILANT'YEV, V.F.;
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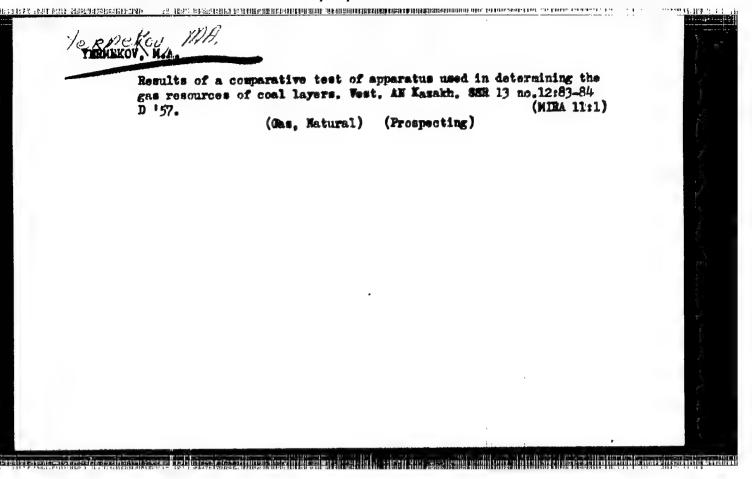
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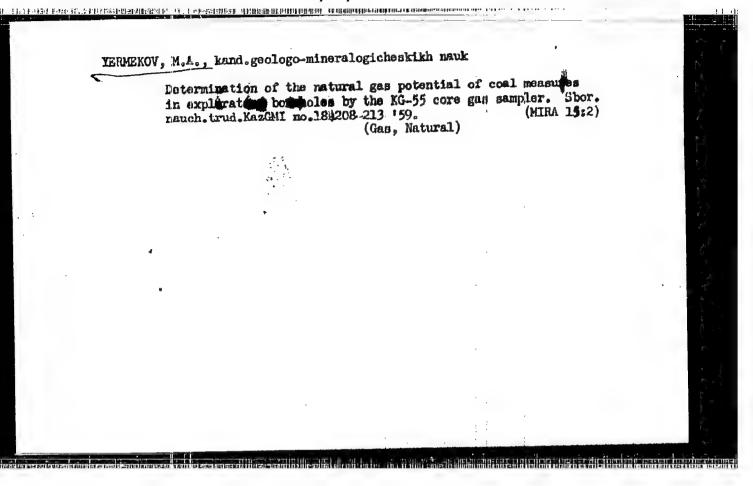
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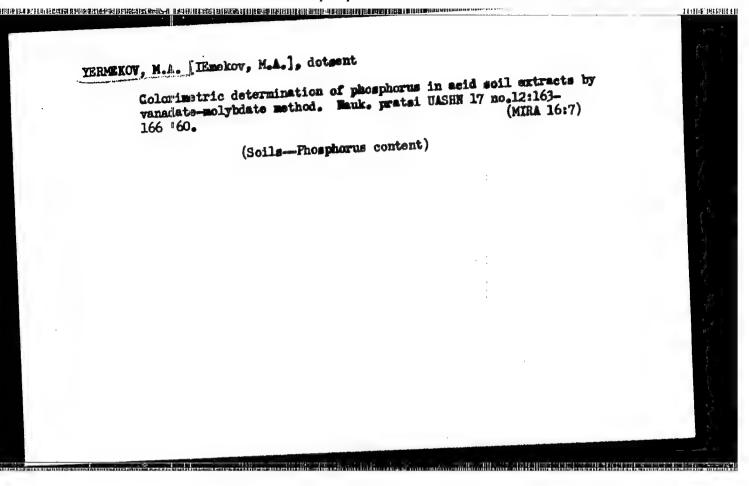


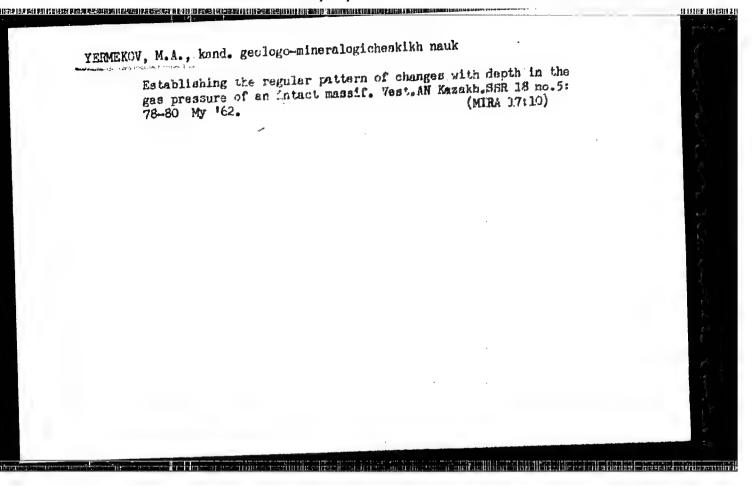


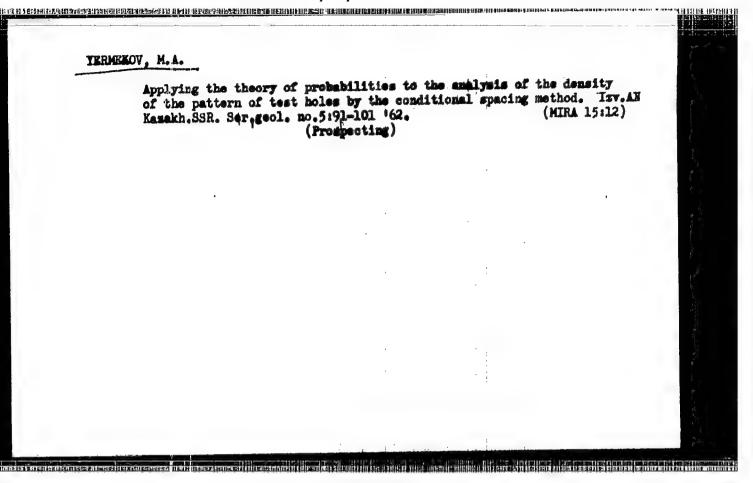
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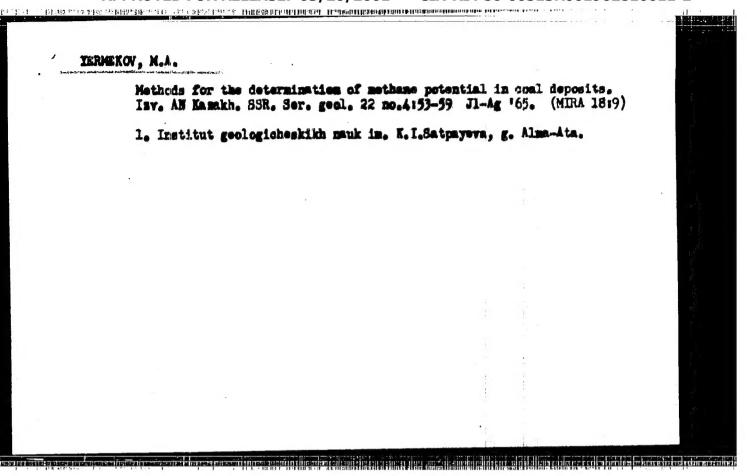
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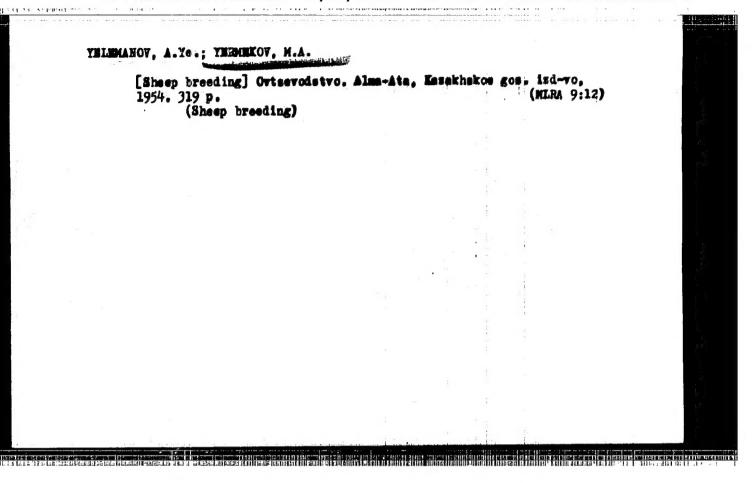


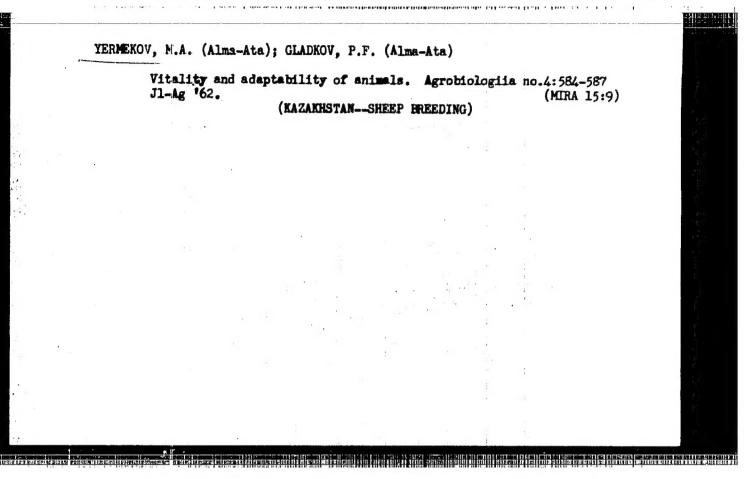












YERMEKOV, M.A., zasluzhennyy deyatel' nauki Kazakhskoy SiR; GLADKOV, P.F., aladshiy nauchnyy sotrudnik; CHUMIN, N.P., mladshiy nauchnyy sotrudnik

Fat-tailed sheep of central Zazakhstan. Zhivotnovodstvo 24 no.9:61-67
S'62. (MIRA-15:12)

1. Kazakhskiy nauchno-issledovatel'skiy institut zhivotnovodstva. (Kazakhstan—Sheep breeds)